

ACOUSTIC SOLUTIONS.



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ACOUSTIC ENCLOSURES



Introduction

Noise is often conveniently defined as a sound which is unwanted by the recipient. Unwanted noise is no longer something that has to be endured, it can and must be controlled.

In any surroundings, the primary cause of complaint due to noise is nearly always linked to excessive sound levels, either within or external to premises. Any problem involving the avoidance of unwanted noise may be tackled by a systematic approach.

Enclosing the sound source can sometimes be the most effective method of noise control. To be most effective the source must be totally enclosed. It is however, necessary with a lot of equipment to provide ventilation for cooling. Unless only small sound reduction is required, any openings for ventilation must not degrade the performance of the enclosure and should, therefore, either contain attenuators or acoustic louvers.

When only a small reduction is required a partial enclosure, which provides natural ventilation, may be sufficient.

Application

Acoustic Enclosures are designed and built for optimum noise control and may be used to enclose the noise, in the case of equipment operations. Complete mechanical isolation between source and enclosure is required. Preferably the machine itself should be vibration isolated from the floor and its services.

The pre-fabricated modular units, enables it to be constructed in a variety of sizes which is suitable for site assembly.



Description

Use

The Acoustic Enclosure, type LMV, is used where both simple and effective sound screening or noise encapsulation is desired. The flexible system makes the machine room walls particularly viable for the construction of separate rooms in production and storage locations as well as offices for shop foremen, controls room, crew's quarters, storage rooms, etc. and for noise encapsulation of machines and production systems by ventilators, compressors, generating systems, etc.

Benefits

The modular construction of Acoustic Enclosure leads to the system being:

- able to be set up and installed on-site
- able to be part of both small as well as large encapsulations
- able to be expanded or changed in step with production expansions, etc.
- able to be set up as an extension of other elements
- able to be delivered either as parts or as a complete job

All in all, it gives great flexibility, which makes the system ideal for countless purposes.

Design

Acoustic Enclosures are modularly designed. The exterior sides of the modules consist of a galvanized steel plate, which is glued onto mineral wool. The modules are also available in perforated steel plates. Assembly is performed via a supplied channel, and the elements can moreover be mounted both vertically (as in the picture) and horizontally.

The elements are supplied in a standard width of 500mm to 1080mm. The elements can be supplied as needed in lengths of up to 3000mm. Adjustments to the elements can easily be performed during installation using an electric saw. LMV can be supplied with protective sheeting.



Description

The acoustic panels consist of outer and inner walls with acoustic infill in between are modularly designed and built to reduce noise or enclose the noise.

Construction

The standard acoustic panels used for both walls and roof are 500mm to 1080mm wide (for 50mm thickness) constructed of an outer wall of galvanized steel sheet metal Ga.16. Acoustic infill is retained behind an inner wall of either perforated or solid galvanized steel sheet metal Ga.22.

The assembly of panels is on site, by others. Safid will provide full details of panel configuration and assembly.

Technical Data

Standard Width (W): 500 mm to 1080 mm (for 50 mm thick)

Standard Thickness (T): 50 / 100 / 150 / 200

Length (L): Up to 2500 mm

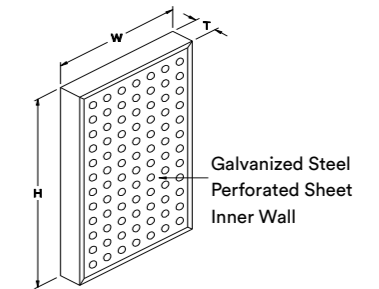
Weight: Approx. 18 kg/m² (for 50 mm thick)

Color: Supplied in galvanized steel finish and epoxy paint in various colors.

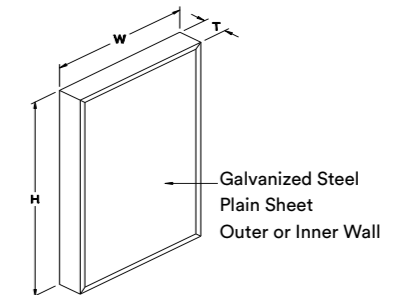
Accessories: Acoustic doors in standard thickness. Assembly rails windows.

Dimensions

LMV-50...200-G-P



LMV-50...200-G-G



Ordering

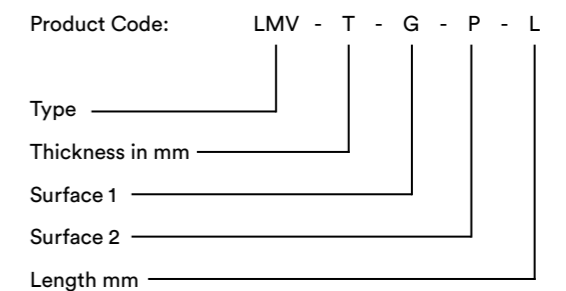


Table 1: Sound Transmission Loss in dB

Type	Octave Centre Frequency, fm in Hz						
	63	125	250	500	1000	2000	4000
LMV - 50 - G - P	17	20	20	24	25	27	32
LMV - 50 - G - G	21	25	29	32	36	38	42
LMV - 100 - G - P	23	22	22	29	29	32	39
LMV - 100 - G - G	28	30	32	39	39	44	49
LMV - 150 - G - P	26	24	31	36	36	42	47
LMV - 150 - G - G	33	37	41	48	48	50	50
LMV - 200 - G - P	28	25	32	34	34	44	49
LMV - 200 - G - G	35	39	42	49	49	50	50

Noise Reduction

The Table shows the sound transmission loss figures ± 3dB for the different types of elements. For elements with epoxy paint, the values for galvanized steel or perforated galvanized steel can be used.

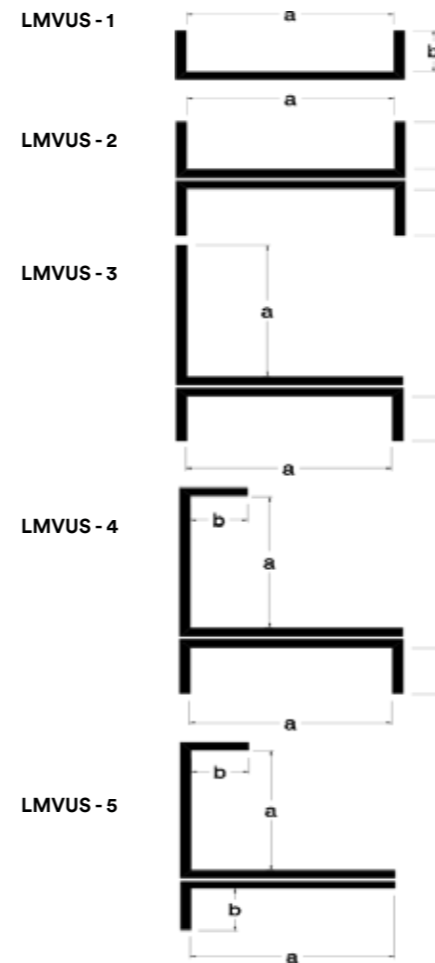
For example. LMV-50-G-P: Plain galvanized steel sheet on one side, and perforated steel sheet on the other side.

Table 2: Selection of Combination

Thickness in mm	Surface 1		Surface 2		
	G	PL	G	P	PL
50	x		x	x	x
50		x		x	x
100	x		x	x	x
100		x		x	x
150	x		x	x	x
150		x		x	x
200	x		x	x	x
200		x		x	x

G = Galvanized Steel
 PL = Epoxy Coated Finish
 P = Perforated Galvanized Steel

LMVUS



Construction Variants

LMVUS - 1 : railing to be mounted horizontally on the floor.

LMVUS - 2 : railing to be mounted on horizontal or vertical position between walls or ceiling panels.

LMVUS - 3 : railing to be mounted on top of the wall panels.

LMVUS - 4 : vertical railing typical of 3 pieces to be mounted in dequence on 3 corners of the wall.

LMVUS - 5 : vertical railing to be mounted on the last corner of the walls during assembly.

Dimensions

Standard Dimensions

a (mm)	b (mm)
55	35
105	35
155	35
205	35

LMVUD



LMVUD : angle railing for exterior edging around on corners of wall and ceiling panels.

Dimensions

Standard Dimensions

a (mm)	b (mm)
85	45
135	45
185	45
235	45



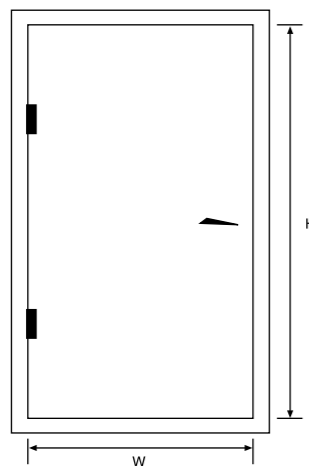
Description

Machine room doors are double walled door panel with mineral wool insulation. Designed to provide access for machine rooms and enclosure.

Construction

Machine room doors are supplied in standard 50 mm thicknesses, and can be installed as needed with 2-layers made-to-measure double glazing. Outer and inner walls are manufactured from galvanized steel sheet metal 3mm thick. Closure by double lever locking devices which can be operated from both sides. Can be supplied with double glass as option.

Dimensions



Standard Sizes

	Doorway Size	
	W (mm)	H (mm)
Standard	605	805
Single Leaf	605	1205
	605	1605
	605	1805
Spec. Single Leaf	800	1961
Double Leaf	1595	1961





SILENCERS



Basic Principle of Sound

Noise is an unavoidable part of everyday life and technological development has resulted in an increase in noise level from machines, factories, traffic etc. It is therefore important that steps towards a reduction in noise are taken, so that noise is not something we have to accept. In connection with this fight against noise, you must have some basic knowledge about how and where is noise generated, transmitted and attenuated in system in order to be able to select the proper principle and products.

This description does not claim to teach you how to calculate and attenuate noise in a ventilation system - there are books available on this.

This description only aims at providing information about a few simple rules and hints, which together with common sense can be enough for simple installations.

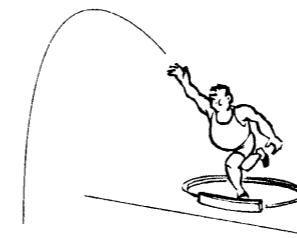
To take a simple analogy: noise transmission consists of waves in a medium, i.e. air, which we can not see. This is very similar to the way waves spread on water.

Let us examine the analogy, to make the comparison clearer:

Source

Waves on Water

We throw a stone onto completely calm water.



Waves in Air

We fire a starter's gun.



Distribution

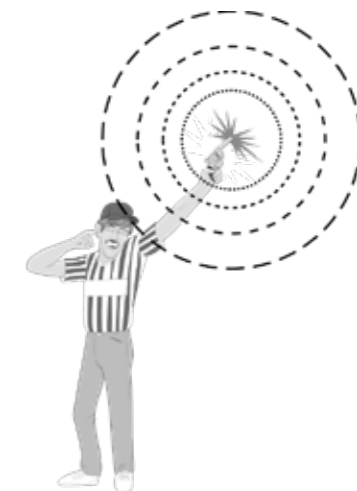
Waves on Water

Waves on water spread out in increasing concentric circles from the centre, where the stone hit the water.



Waves in Air

Sound waves spread out in the air, in all directions, in an increasing ball from the centre, i.e. the gun.



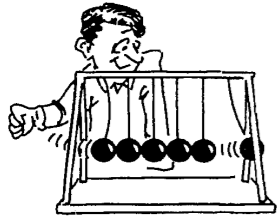
Energy Transport

Waves on Water

Kinetic energy is transmitted from molecule to molecule in the water. They bounce against each other. Molecules move back and forwards. Energy spreads from the source.

Waves in Air

Kinetic energy is transmitted from molecule to molecule in the air. They bounce against each other, and move back and forwards. Energy spreads from the source.



Distance

Waves on Water

When waves depart from the centre, where the stone hit, the wave height becomes lower and lower, until they are invisible. The water is calm again.

Waves in Air

When sound waves depart from the source, the starter's gun, wave movement drops off and the sound becomes weaker and weaker until it can no longer be heard.



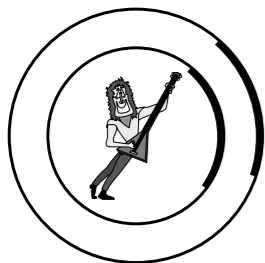
Intensity

Waves on Water

The energy which started the wave propagation, or the power needed to keep it going, is distributed across and increasing area as the distance, the radius, increases

Waves in Air

The energy which started the wave propagation, or the power needed to keep it going, is distributed across an increasing volume as the distance, the radius, increases.



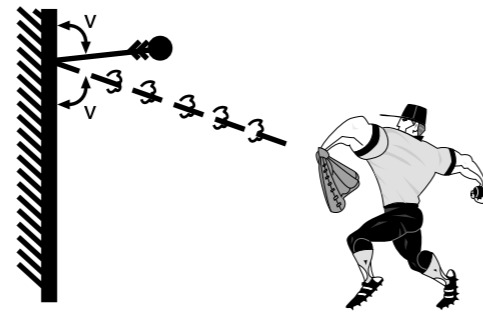
Obstruction in the Way

Waves on Water

If waves in water encounter the side of a boat or jetty, they will be reflected at the same angle as they met the obstruction.

Waves in Air

If waves in air encounter a wall, they will be reflected at the same angle as they met the obstruction.



In the same way as when you bounce a ball on the wall.

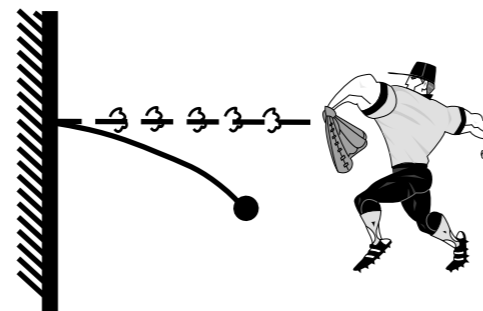
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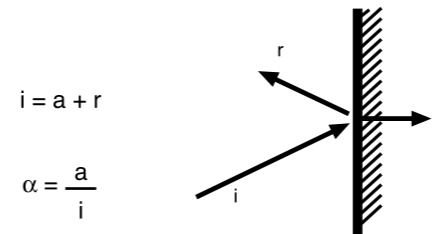
Absorption

Sound can be absorbed

When sound waves meet a soft, porous wall (mineral wool etc.), the vibrating molecules penetrate the surface layer, and are then braked by friction against the material fibres.

The part of the energy which is thus absorbed is converted to heat in the material, and the rest is reflected back into the room. This type of damping, where the sound is braked by the soft surface layer, is referred to as porous absorption.

The sound absorption ability of different materials varies. This property is expressed as the sound absorption factor of the material.



If nothing is absorbed, everything is reflected, then $a = 0$ which makes $\alpha = 0$:

$i = a + 0$ $\alpha = \frac{a}{a} = 1$

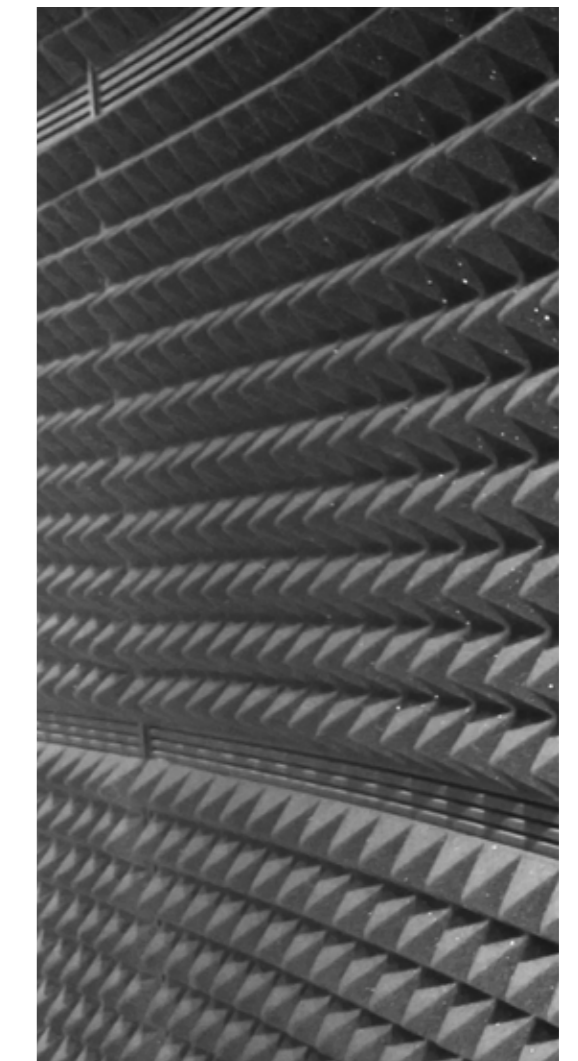
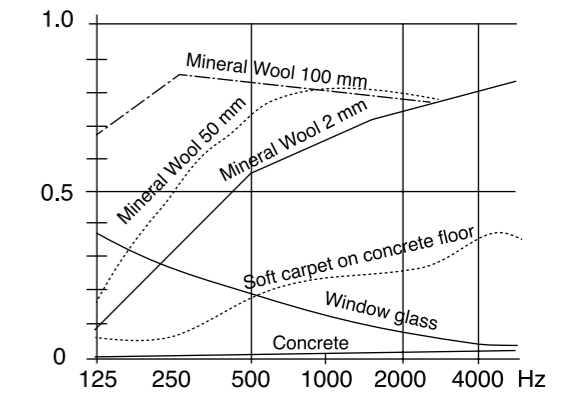
If nothing is absorbed, everything is reflected, then $a = 0$ which makes $\alpha = 0$:

$i = 0 + r$ $\alpha = \frac{0}{i} = 0$

An open window can be said to have $a = 1$, all sound from the room which arrives at the window disappears out!

In hard materials, such as concrete or marble surfaces, virtually no sound energy is absorbed, everything is reflected and the a value is near to zero. In rooms with hard surfaces, the sound bounces for a long time before it dies out. The room has a long reverberation time and we get a strong, unpleasant echo. The sound level caused by normal sound sources becomes high.

In soft materials, such as thick mineral wool boards, the opposite happens. The a value is close to 1. Sometimes, excessively damped, soft rooms are unsuitable "You can't hear what you say". Avoid extremes - the reverberation time in a room should be chosen to suit the activities there.



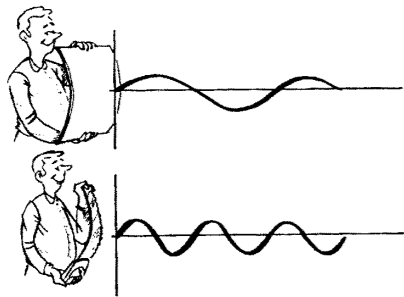
Frequency and Wavelengths

As we see in the tables above, the damping ability varies with the frequency of sound. It could be a good idea to describe the concept of frequency in greater detail.

A sound source influences the surrounding air, and makes it vibrate. The character of the sound depends on the variations in pressure which occur in the air.

Let us assume that the sound source is a vibrating plate - the changes in pressure, or the sound will then have the same frequency as the vibrations in the plate. The strength of the sound will depend on the amount that the plate vibrates, i.e. the amplitude of the movement. Let us start off with that:

If there is only one note, of a single frequency, the pressure will vary sinusoidally, so a pure note is referred to as a sine wave.



The characteristics of sound propagation are:

- frequency (f), which is measured in Hertz, Hz, (s⁻¹), (and specifies the number of times a second that a new sound wave arrives).
- wave length (λ, "lambda"), which is measured in metres, m, (and specifies the distance between two similar points on the curve).

- speed of sound (c) which is measured in m/s, (and specifies the speed of movement of the sound wave).

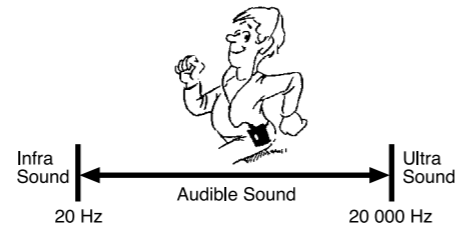
These three variables have the following relationship:

$$c = f \cdot \lambda$$

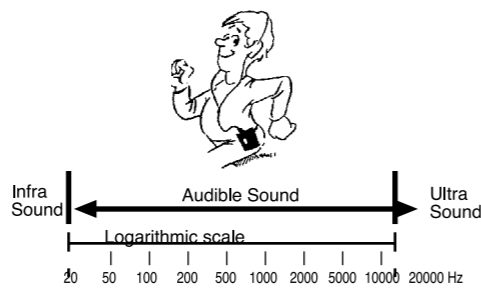
The speed of sound in air is also a function of pressure and temperature.

At normal air pressure and + 20°C:
c ≈ 340m/s.

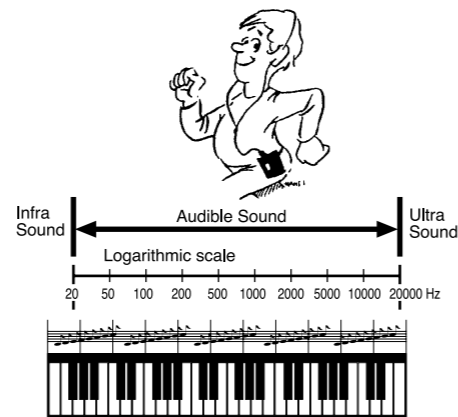
A young person with normal hearing can hear sounds at frequencies from 20-20 000 Hz, i.e. (in air) at wavelengths ranging from 17 m (at 20 Hz) to app. 17mm (at 20 kHz).



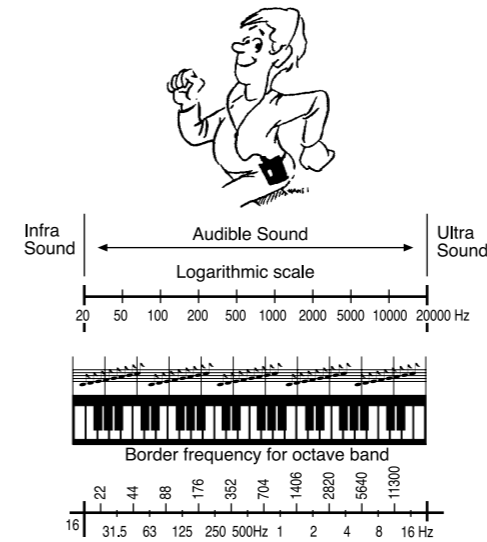
We perceive changes in sound frequency on a logarithmic scale, i.e. it is the relative frequency and not the difference in Hz which determines how a change in note is perceived. A doubling of frequency is perceived as being the same, irrespective of whether it is a change from 100 to 200 Hz, 1000 to 2000 Hz or 10 to 20 kHz.



The logarithmic scale is usually sub-divided into octaves. i.e. in scales where the top note is twice the frequency of the bottom note. This has been customary in music for a long time.

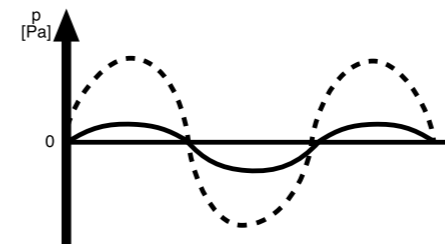


Frequency and Wavelengths



The Concept of Decibel

The stronger the sound is, the harder the particles of air will bump into each other



Sound pressure changes in the audible area can vary within very wide limits. Some sounds are so weak that we can not hear them. The so-called audible limit varies with frequency and is 20 mPa at about 1000 Hz.

Other sounds are so loud that we risk hearing damage. The pain limit, the sound pressure which causes pain in your ears also varies with frequency, but is about 20 Pa at 1000 Hz. This means that it is a million times louder than the weakest sound we can perceive.

We also perceive changes in sound pressure on a logarithmic scale. A sound level concept using the decibel (dB) as the unit, has been created to express comparable values.

The dB unit, which is used in many different applications, is generally defined as: $10 \cdot \log (X/X_0)$, where X is the unit measured, i.e. the sound pressure, and X₀ is a reference level expressed in the same units. The relationship of X/X₀ is thus dimensionless. The reference level from which the dB unit is specified, is given instead. This means that you generally express the level in dB (above X₀).

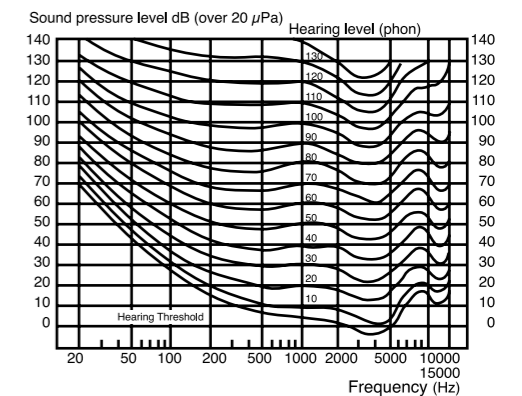
Our Perception of Sound

We react differently to two sounds which have the same sound pressure level and different frequencies.



Curves which describe how people normally perceive sounds of varying strength and frequency have been constructed through experiments on large numbers of volunteers. These so-called hearing level curves are designated by the sound pressure level for each curve at a frequency of 1 kHz. The unit used for the curves is the phon.

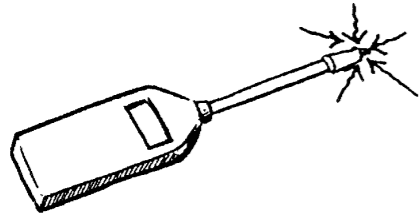
Hearing Level Curves



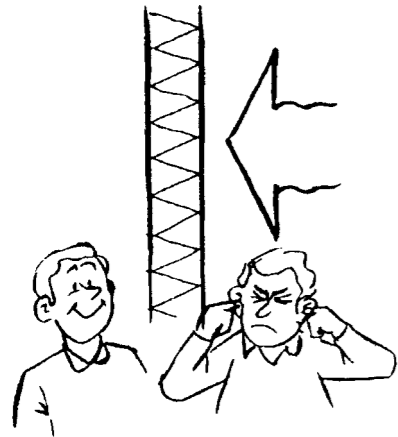
Example:

The sound pressure level 70 dB at 50 Hz is normally perceived as being as loud as 50 dB at 1000 Hz.

Sound Levels

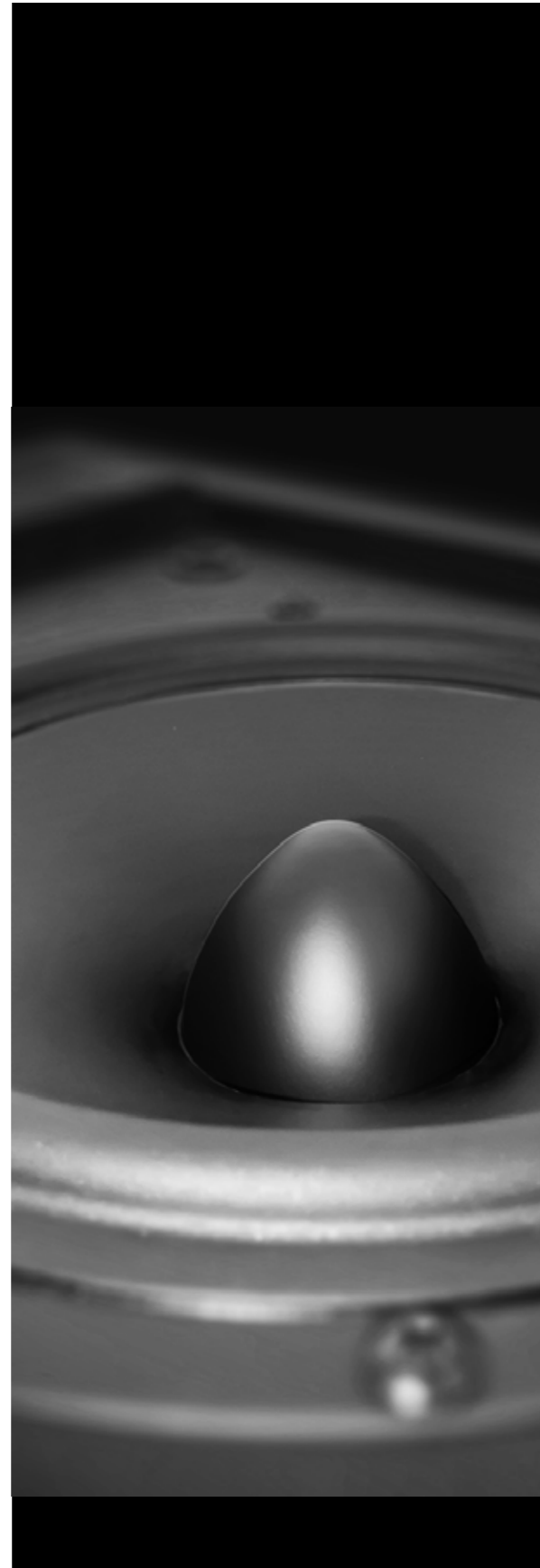
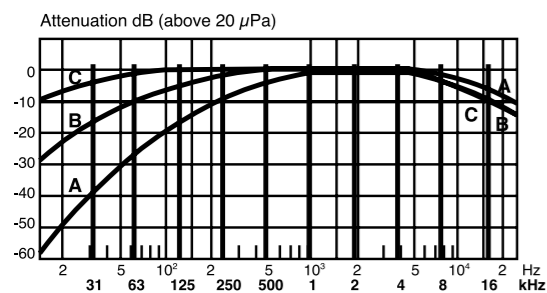


Several methods are used to compare the disturbance caused by two different sounds, and where the perception of the ear to noise has been modelled.



The simplest way is to compare their "weighted" sound levels. The incoming sound is filtered in an electronic filter to reduce the components, mostly the low-frequency components, where the ear is not so sensitive, and amplify the components between 1 and 4 kHz, where we are most sensitive.

Sound meters usually have three electronic filters, A-, B- and C-filter. The A-filter is mostly used these days, where the result, the "weighted" sound level, is expressed in dB (A).



Sound

Sound is such a common part of everyday life that we rarely appreciate all of its functions. It provides enjoyable experiences such as listening to music or to the singing of birds. It enables spoken communication and it can alter or warn us - for example, with the ringing of a telephone, or a wailing siren. Sound also permits us to make quality evaluations and diagnoses - the chattering valves of a car, a squeaking wheel, or a heart murmur.

Sound and Noise

Yet, too often in our modern society, sound annoys us. Many sounds are unpleasant or unwanted - these are called noise. However, the level of annoyance depends not only on the quality of the sound, but also our attitude towards it.

For example the type of music enjoyed by some people could be regarded as noise by others, especially if it is loud. But sound doesn't need to be loud to annoy. A creaking floor, a scratch on a record, or the intermittent sound of a dripping tap can be just as annoying as loud thunder. The judgement of loudness will also depend on the time of the day. For example, a higher level of noise will be tolerated during the day than at night.

Good Acoustic Design

Adequate noise control in a duct system is not difficult to achieve during the design of the system, providing the basic noise control principles are understood. Despite the addition of noise control items in more and more building designs, complaints about HVAC system noise are still common. Investigations into noise complaints by acoustical professionals have found that, in many cases, the correct equipment and materials were used, but they were not properly integrated into a quiet system.

Virtually every survey on building comfort finds that excessive HVAC system noise levels are responsible for more complaints than any other aspect of the building environment. To minimize the possibility that design decisions could cause noise problems, the design team must consider the acoustical impacts of all design decisions, whether they are part of the schematics, design development, working drawings, or construction administration phases of the project.

Therefore, noise control design should begin during the schematic and design development phases and continue throughout the entire design process.

Noise Control Principles

There are three distinct stages to the noise control process:

1. Source.
2. Transmission.
3. Reception

Noise control problem involves examining the noise sources,(fan noise, duct noise, diffuser noise, and building noise) the sound transmission paths, and the receivers. For most HVAC systems, the sound sources are associated with the building mechanical and electrical equipment.

Noise travels from the source to the receiver through many possible sound transmission paths,(structure-borne path through floor, airborne path through supply air system, duct breakout from supply air duct, airborne path through return air system, and airborne path through mechanical equipment room wall). Sound sources are the components that either generate noise, like electric motors, or produced noise when air passes by them, like dampers or diffusers. Sound receivers are generally the occupant of the building.

The noise control engineers are most often constrained to modifying the sound transmission paths as a mean of achieving the desired sound levels in occupied areas of a building.

Definitions

Attenuation

The reduction of sound level per unit distance by divergence, diffusion, absorption, or scattering.

A-weighted Sound Level

The sound level measured using the A-weighting network of a sound level meter. For broadband sounds, the A-weighted sound level indicates approximate relative loudness.

Background Noise

It is the irreducible noise level measured in the absence of any building occupants when all of known sound sources have been turned off.

Breakout Noise

The transmission of fan or air system noise through duct walls.

Criteria

Noise levels which are subjectively or objectively acceptable in a given environment. The most commonly used criteria are Noise Criteria Curves (NC Levels), Noise Rating Curves (NR Levels) and dB(A).

Decibel (dB)

Commonly, the unit used to measure sound. It is used to quantify both sound pressure level and sound power level.

Direct SPL

Noise which is transmitted directly from a source (i.e. a grille or diffuser) without reflection.

Ductborne Noise

Noise which is transmitted along ductwork, both upstream and downstream of fan.

Flanking Noise (Breakout)

Noise transmitted through a barrier, often a fan casing or ductwork. Any indirect noise path which tends to devalue noise control measures used to reduce transmission along the more obvious paths.

Frequency (Hz.)

The pitch of sound. The number of sound pressure waves arriving at a fixed point per second.

Insertion Loss

A measure of the noise reduction capability of an attenuator (sometimes of a partition) so named.

After the method of testing where a section of ductwork is replaced by an attenuator between two test rooms. One room contains the noise source and the other the sound level measuring equipment. The difference in recorded noise level is said to be the insertion loss due to the insertion of the attenuator in the system.

Noise Outlet

Usually a grille or a diffuser. Any opening acting as a terminal element on either an extract or supply system.

Octave Bands

Subdivisions of the frequency range each identified by its mid (or centre) frequency. By international agreements these comprise 63, 125, 250, 500, 1k, 4k, and 8k Hz. and sometimes 31.5 Hz.

Regenerated Noise

Noise in addition to that produced by the fan, caused by air passing over fixed duct elements such as blades on grilles, dampers, air turns, splitters in attenuators, etc.

Reverberant SPL

Noise which is transmitted by reflection off room surfaces.

Reverberant Time

A measurement of the acoustic "reflectiveness" of a room.

Sound Power Level (SWL)

A theoretical assessment of sound produced at source calculated from the measured sound pressure levels at known distances from the source under known acoustic conditions. A level which depends only on the source and is independent of the environment or location. The sound power level of a fan is therefore very useful information since any level quoted can be compared directly with data from any other manufacturer.

Sound Pressure Level (SPL)

A measured sound level which is an indication only of the noise produced at source since environmental factors such as reverberation and distance from the source have affected the measurement. The sound pressure level of a fan is not very useful since environmental factors apparent when the unit was measured may or may not be present in the actual location of the plant.

Acoustic Design Procedures

Good acoustical design requires broad cooperation in the areas of architecture, structural, mechanical, electrical engineering, and acoustics. Delaying the acoustical design until after the structural system design is essentially complete sometimes leaves the design team with little flexibility in selecting and locating cost-effective noise control equipment and materials.

In order to effectively deal with each of the different sound sources and related sound paths associated with an HVAC system, the following design procedures are suggested :

1. Determine the design goal for HVAC system noise for each critical area according to its use and construction. Use Table 14 to specify the desirable NC levels.
2. Relative to equipment that radiates sound directly into a room, select equipment that will be quiet enough to meet the desired design goal.
3. If central or roof-mounted mechanical equipment is used, complete an initial design and layout of the HVAC system, using acoustical treatment where it appears appropriate.
4. Starting at the fan, appropriately add the sound attenuations and sound power levels associated with the central fan, and duct elements between the central fan and the critical room to determine the corresponding sound pressure levels in the room. Be sure to investigate the supply and return air paths. Investigate possible duct sound breakout when central fans are adjacent to the critical room or roof-mounted fans are above the critical room.
5. If the mechanical equipment room is adjacent to the critical room, determine the sound pressure levels in the room associated with sound transmitted through the mechanical equipment room wall.
6. Add the sound pressure levels in the critical room that are associated with all of the sound paths between the mechanical equipment room or roof-mounted unit and the critical room.

7. Determine the corresponding NC level associated with the calculated total sound pressure levels in the critical room.

8. If the NC level exceeds the design goal, determine the octave frequency bands in which the corresponding sound pressure levels are exceeded and the sound paths that are associated with these octave frequency bands.

9. Redesign the system, adding additional sound attenuation to the paths which contribute to the excessive sound pressure levels in the critical room.
10. Repeat steps 4 through 9 until the desired design goal is achieved.

11. Steps 3 through 10 must be repeated for every room that is to be analyzed.

12. Make sure that noise radiated by outdoor equipment will not disturb adjacent properties.

13. With respect to outdoor equipment, use barriers when noise associated with the equipment will disturb adjacent properties.

14. If mechanical equipment is located on upper floors or is roof-mounted, vibration isolate all reciprocating and rotating equipment. It may be necessary to vibration isolate mechanical equipment that is located in the basement of the building.

A sound analysis should be carried out starting from the fan or noise source having ducted connections to the room of interest.

It is strongly recommend that sound level requirements for NC 30 or below be calculated out by SAFID so as to ensure a complete check against noise criteria levels.

Fan In-Duct Sound Power Level

Obtain from the fan manufacturer's catalogue information, or calculate the approximate In-duct Sound Power Level from Table 1.

In both case the approximate duty of the fan needs to be known.

These figures are inserted in line a. Some manufacturers present noise data as a Sound Pressure Level which needs to be converted by applying the relevant correction factor.

Duct System Between the Fan and the Critical Noise Outlet

Select the most critical noise outlet in the duct system, normally the noise outlet nearest to the fan, and estimate the sound power reduction which occurs along the duct path to this outlet and the outlet itself. Using the following information assess the total duct attenuation.

Straight unlined sheet metal ducts provide a degree of attenuation. This is frequency dependent and varies with the minimum duct dimension and duct length. Approximate attenuation of straight unlined rectangular sheet metal ducts per meter run is shown in Table 2.

To avoid noise breakout problems in the duct attenuation taken should be limited to approximately 15dB.

Circular sheet metal duct attenuation shown in Table 3. Bends provide attenuation as shown in Tables 4 and 5. Duct and bend attenuation figures should be entered against lines b.

At low frequencies some of the sound power on reaching the critical noise outlet is reflected back along the duct. The degree of attenuation due to this phenomenon is dependent on frequency and the total area of the outlet. The attenuation from Table 6 is inserted in line c.

The Sound Power Level leaving the critical outlet is obtained from $e=a-(b+c)$

Calculate the Room Effect

In a room the sound pressure waves will reach the listener along two paths:

1. Directly, reducing as the (distance)² from the noise source, known as the Direct Sound Pressure Level.
2. By multiple reflections off the room surfaces and room contents, which will depend upon the size of the room and the reverberation time, known as the Reverberant Sound Pressure Level.

To estimate the Direct Sound Pressure Level.

Calculate the percentage of the total sound leaving the critical noise outlet. This is approximately equal to the percentage of the fan air volume which passes through the critical outlet.

Table 7 gives the factors to be inserted in line f.

Estimate the distance between the nearest listening position and the critical outlet, and using Table 8, insert the distance factors in line g. Unless the specification states otherwise, the commonly applied distance is 1.5 meters.

By examining the position of the nearest outlet in relation to the walls and ceiling of the room will affect the resultant sound pressure level, due to directivity. Select the location type (A, B, or C) using Table 9, which is closest to matching the position of the critical outlet in the room.

Using the charts for the chosen location type and outlet area, insert the factors obtained in line h.

The Direct Sound Pressure Level in the room in line i is equal to the sum of the Sound Power Level leaving the Critical Outlet in line e and lines f g h.

To estimate the Reverberant Sound Pressure Level.

For the fan system in question, Calculate the percentage of the sound emerging from all the noise outlets in the room served by the fan.

This approximates to the percentage of the fan air volume serving the room under investigation.

Using Table 10 insert the factor in line k.

The amount of reflection or absorption of the sound emerging from the noise outlets depends upon the volume and the reverberation time (which is a function of the amount of absorption) of the room. Table 11 and 12 give the factors related to these which are inserted in lines l and m respectively.

The factors tabulated at each Octave Band in lines k,l and m are now added together to give the Total Reverberant Factors.

The Reverberant sound Pressure level (line o) in the room is equal to the sum of the Sound Power Level leaving the Critical Outlet (line e) and the Total Reverberant Factors (lines k + l + m).

To arrive at the Combined Sound Pressure Level, it is necessary to logarithmically sum the Reverberant Sound Pressure Level and the Direct Sound Pressure Level. This can be simplified by using Table 13. The combined pressure level can then be entered in line p.

Required Insertion Loss

The specification will usually give a design criteria for various area function; where one is not given, Table 14 can be used.

The required or selected criterion is inserted in line q.

If the Combined Sound Pressure Level exceeds the Criterion in any Octave Band, then the difference is the Insertion Loss required from the attenuator (line r).

To allow the possible addition of noise from other sources a safety margin of typically 3dB may be added.

The attenuator can now be selected to meet the parameters of insertion loss, physical size and the pressure loss. The Insertion Loss figures are placed in line s as a final check.

The above analysis method takes no account of regenerated noise from attenuators or ductwork elements.

Similarly, it is not possible to deal with the method of selecting attenuators for high pressure systems which commonly have terminal devices that generate noise and often have some attenuation capability

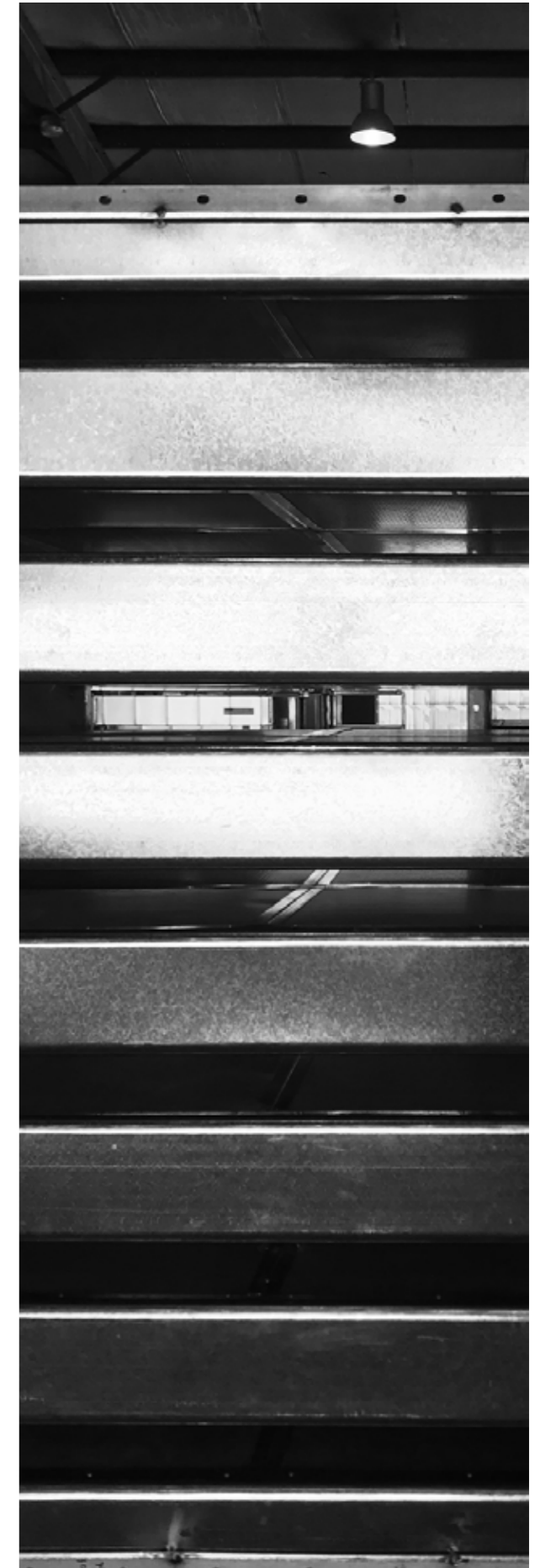
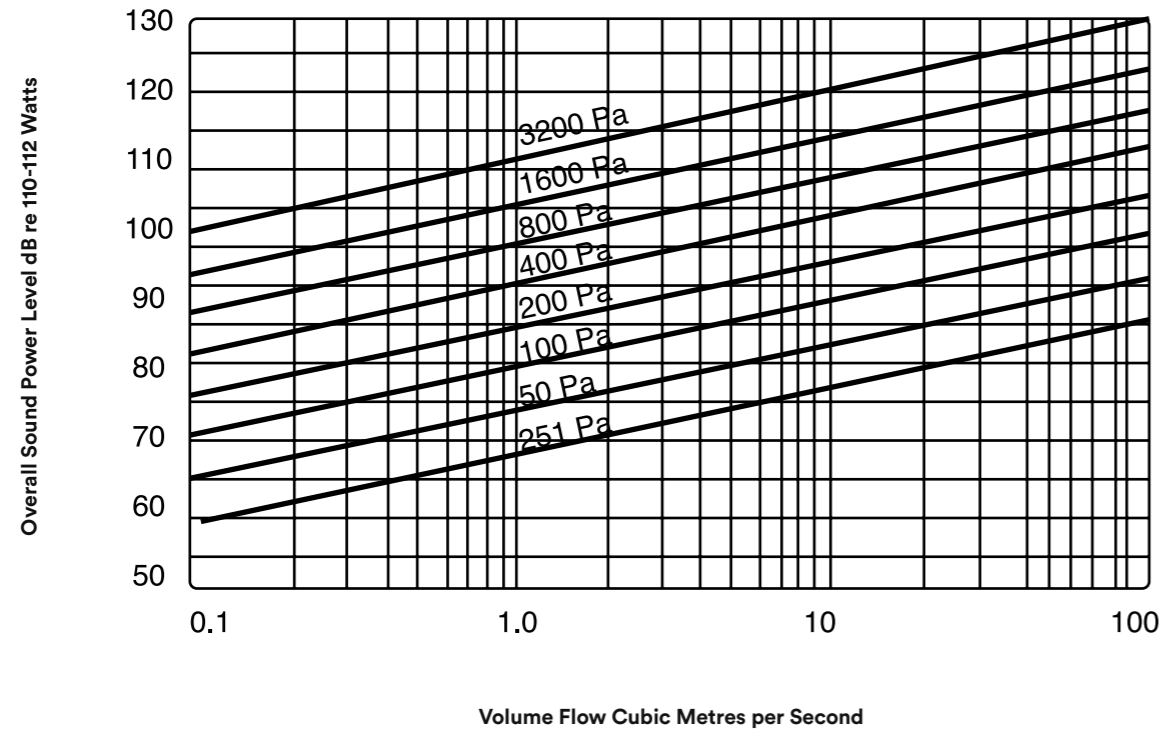


Table 1: In-Duct SWL of the Fan



Spectrum Correction

	Octave Centre Frequency (f_m in Hz)							
	63	125	200	500	1k	2k	4k	8k
Forward Curved Centrifugal	-2	-7	-12	-17	-22	-27	-32	-37
Backward Curved Centrifugal	-7	-8	-7	-12	-17	-22	-27	-32
Axial	-5	-5	-6	-7	-8	-8	-14	-17

Table 2: Attenuation of Straight Unlined Rectangular Sheet Metal Ducts - (dB/m)

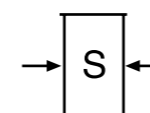
	Min. Duct Dimension S (mm)	Octave Centre Frequency (f_m in Hz)							
		63	125	250	500	1k	2k	4k	8k
000 - 200	0.6	0.6	0.45	0.3	0.3	0.3	0.3	0.3	0.3
201 - 400	0.6	0.6	0.45	0.3	0.2	0.2	0.2	0.2	0.2
401 - 800	0.6	0.6	0.3	0.15	0.15	0.15	0.15	0.15	0.15
801 - 1600	0.3	0.15	0.15	0.1	0.06	0.06	0.06	0.06	0.06

Table 3: Attenuation of Straight Unlined Circular or Round Sheet Metal Ducts - (dB/m)

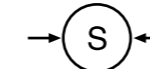
	Min. Duct Dimension S (mm)	Octave Centre Frequency (f_m in Hz)							
		63	125	250	500	1k	2k	4k	8k
000 - 180	0.03	0.03	0.05	0.05	0.1	0.1	0.1	0.1	0.1
181 - 380	0.03	0.03	0.03	0.05	0.07	0.07	0.07	0.07	0.07
381 - 760	0.02	0.02	0.02	0.03	0.05	0.05	0.05	0.05	0.05
761 - 1520	0.01	0.01	0.01	0.02	0.02	0.02	0.02	0.02	0.02

Table 4: Attenuation of Mitred Bends Without Turning Vanes or with Short Chord Turning Vanes (Rectangular Ducts) - dB

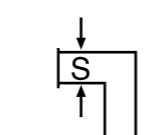
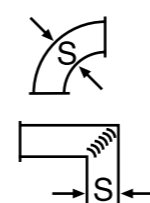
	Min. Duct Dimension S (mm)	Octave Centre Frequency (f_m in Hz)							
		63	125	250	500	1k	2k	4k	8k
000 - 200	0	0	0	0	6	8	4	3	
201 - 400	0	0	0	6	8	4	3	3	
401 - 800	0	0	6	8	4	3	3	3	
801 - 2000	0	6	8	4	3	3	3	3	

Table 5: Attenuation of Radiussed Bends or Mitred Bends with Long Chord Turning Vanes (Circular or Rectangular Ducts) - dB

	Min. Duct Dimension S (mm)	Octave Centre Frequency (f_m in Hz)							
		63	125	250	500	1k	2k	4k	8k
000 - 250	0	0	0	0	1	2	3	3	
251 - 500	0	0	0	1	2	3	3	3	
501 - 1000	0	0	1	2	3	3	3	3	
1001 - 2000	0	1	2	3	3	3	3	3	

ROOMSIDE ANALYSIS

Table 6: Outlet Reflection (dB)

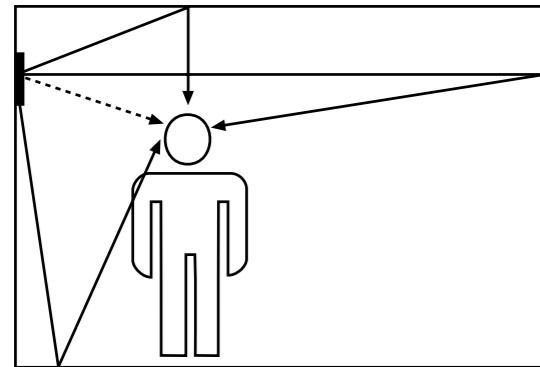
Outlet Area -cm ²	Octave Centre Frequency (f _m in Hz)				
	63	125	250	500	1k
100	20	15	10	6	3
	19	14	9	5	2
	18	13	8	4	1
	17	12	7	3	
	16	11	6	2	
500	14	10	5	2	0
	13	9	4	1	
	12	8	3	1	
	11	7	3	1	
	10	6	2	1	
1000	9	5	2	0	0
	8	4	1	0	
	7	3	1	0	
	6	2	0	0	
	5	1	0	0	
5000	4	1	0	0	0
	3	0	0	0	
	2	0	0	0	
	1	0	0	0	
	0	0	0	0	

Table 7 : Percentage of Total Sound Factors (dB)

-20	1%
-19	
-18	
-17	2
-16	
-15	3
-14	4
-13	5
-12	
-11	
-10	10
-9	
-8	
-7	20
-6	
-5	
-4	
-3	50
-2	
-1	
0	100

Table 8 : Distance Factors (dB)

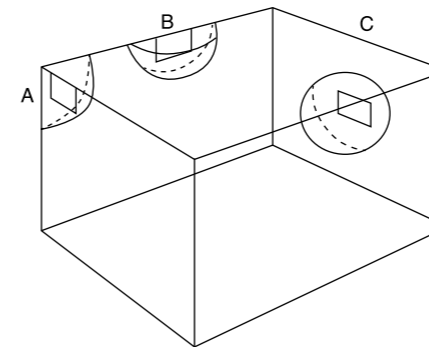
-10	
-11	1 meters
-12	
-13	
-14	1.5
-15	
-16	2
-17	
-18	
-19	
-20	3
-21	
-22	4
-23	
-24	
-25	5
-26	6
-27	
-28	7
-29	8
-30	9



..... Direct
 → Reverberant

ROOMSIDE ANALYSIS

Table 9: Directivity Factor (dB)



Type B	Junction of Two Room Surfaces				Octave Centre Frequency (Hz)
Outlet Area (cm ²)					
	10	100	1000	10000	
	+6		+7	+8	63
	+6	+7	+8		125
	+6	+7	+8	+9	250
	+6	+7	+8	+9	500
	+7	+8	+9		1k
	+7	+8	+9		2k
	+7	+8	+9		4k
	+8	+9			8k

Type C	Junction of Two Room Surfaces					Octave Centre Frequency (Hz)	
Outlet Area (cm ²)							
	10	100	1000	10000	100000		
	+3		+4	+5	+6	+7	63
	+3	+4	+5	+6	+7	+8	125
	+3	+4	+5	+6	+7	+8	250
	+3	+4	+5	+6	+7	+8	500
	+4	+5	+6	+7	+8	+9	1k
	+4	+5	+6	+7	+8	+9	2k
	+5	+6	+7	+8	+9		4k
	+7	+8	+9				8k

Table 10: Percentage of Total Sound Factors (dB)

-20	1%
-19	
-18	
-17	2
-16	
-15	3
-14	4
-13	5
-12	
-11	
-10	10
-9	
-8	
-7	20
-6	
-5	
-4	
-3	50
-2	
-1	
0	100

Table 11: Room Volume Factor (dB)

+10	
+9	3
+8	
+7	5
+6	
+5	
+4	10
+3	
+2	
+1	20
0	
-1	
-2	
-3	50
-4	
-5	
-6	100
-7	
-8	
-9	200
-10	
-11	
-12	
-13	500
-14	
-15	
-16	1000
-17	
-18	
-19	2000
-20	
-21	
-22	
-23	5000
-24	
-25	
-26	10000
-27	
-28	

Table 12: Reverberation Time Factors (dB)

-11	
-10	
-9	
-8	
-7	
-6	
-5	
-4	
-3	Average Furnishing
-2	
-1	
0	Limited Furnishing
+1	
+2	
+3	No Furnishing
+4	
+5	
+6	Very Hard Surface High Ceilings
+7	
+8	
+9	
+10	
+11	

Table 13: Addition of Sound Pressure Levels (dB)

Difference in SPLs	Add to larger SPL
0 to 1	+3
2 to 3	+2
4 to 9	+1
10 and above	+0

Table 14: Recommended Design Criteria for Various Area Functions

Situation	NC
Section 1 - Studios and Auditoria	
Sound Broadcasting (drama)	15
Sound Broadcasting (general), TV (general), Recording Studio	20
TV (audience studio)	25
Concert Hall, Theatre	20 - 25
Lecture Theatre, Cinema	25 - 30
Section 2 - Hospitals	
Audiometric Room	20 - 25
Operating Theatre, Single Bed Ward	30 - 35
Multi-bed Ward, Waiting room	35
Corridor, Laboratory	35 - 40
Wash Room, Toilet, Kitchen	35 - 45
Staff Room, Recreation Room	30 - 40
Section 3 - Hotels	
Individual Room, Suite	20 - 30
Ballroom, Banquet Room	30 - 35
Corridor, Lobby	35 - 40
Kitchen, Laundry	40 - 45
Section 4 - Restaurants, Shops and Stores	
Restaurant, Department Store (upper floor)	35 - 40
Club, Public House, Cafeteria, Canteen, Retail Store (main floor)	40 - 45
Section 5 - Offices	
Boardroom, Large Conference Room	25 - 30
Small Conference Room, Executive Office, Reception Room	30 - 35
Open Plan Office	35
Drawing Office, Computer Suite	35 - 45
Section 6 - Public Buildings	
Court Room	25 - 30
Assembly Hall	25 - 35
Library, Bank, Museum	30 - 35
Wash Room, Toilet	35 - 45
Swimming Pool, Sports Arena	40 - 50
Garage, Car Park	55
Section 7 - Ecclesiastical and Academic Buildings	
Church, Mosque	25 - 30
Classroom, Lecture Theatre	25 - 35
Laboratory, Workshop	35 - 40
Corridor, Gymnasium	35 - 45
Section 8 - Industrial	
Warehouse, Garage	45 - 50
Workshop (light engineering)	45 - 55
Workshop (heavy engineering)	50 - 65
Section 9 - Private Dwelling (Urban)	
Bedroom	25
Living Room	30

Calculation Sheet

SAFID Acoustics

Project:
Client:
Contractor:
Engineer:

Total Air Flow (M³/s)

Source Sound power Level

Smallest Ducts Dimension (mm)	<input type="text"/>	Length (mm)	<input type="text"/>
	<input type="text"/>		<input type="text"/>

Radiused Elbows Width (mm)	<input type="text"/>	Qty.	<input type="text"/>
	<input type="text"/>		<input type="text"/>

Additional Attenuation		<input type="text"/>
<input type="text"/>	<input type="text"/>	<input type="text"/>

Outlet Reflection	Length (cm)	Width (cm)
<input type="text"/>	<input type="text"/>	<input type="text"/>

SWL Leaving System

Percentage Leaving Outlet	M ³ /s	<input type="text"/>
Distance from Outlet to Listener (m)	<input type="text"/>	<input type="text"/>
Directivity	Centre of Wall or Ceiling	<input type="text"/>

Direct SPL

Percentage Leaving Outlet	M ³ /s	<input type="text"/>
Room Volume	Length x Width (m ²)	Height (m)
Reverberation Time	<input type="text"/>	Seconds

Reverberant SPL

Combined SPL

Criterion NC / NR / dBA	NC
Add dB Safety Factor	<input type="text"/>

Required Insertion Loss

Required Insertion Losses dB
Selected Insertion Losses dB
Air Generated Sound Power Level

Roomside Analysis Calculations

Date:
Building:
Equipment No:
Offer No:

Octave Centre Frequency							
63	125	250	500	1k	2k	4k	8k

<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>
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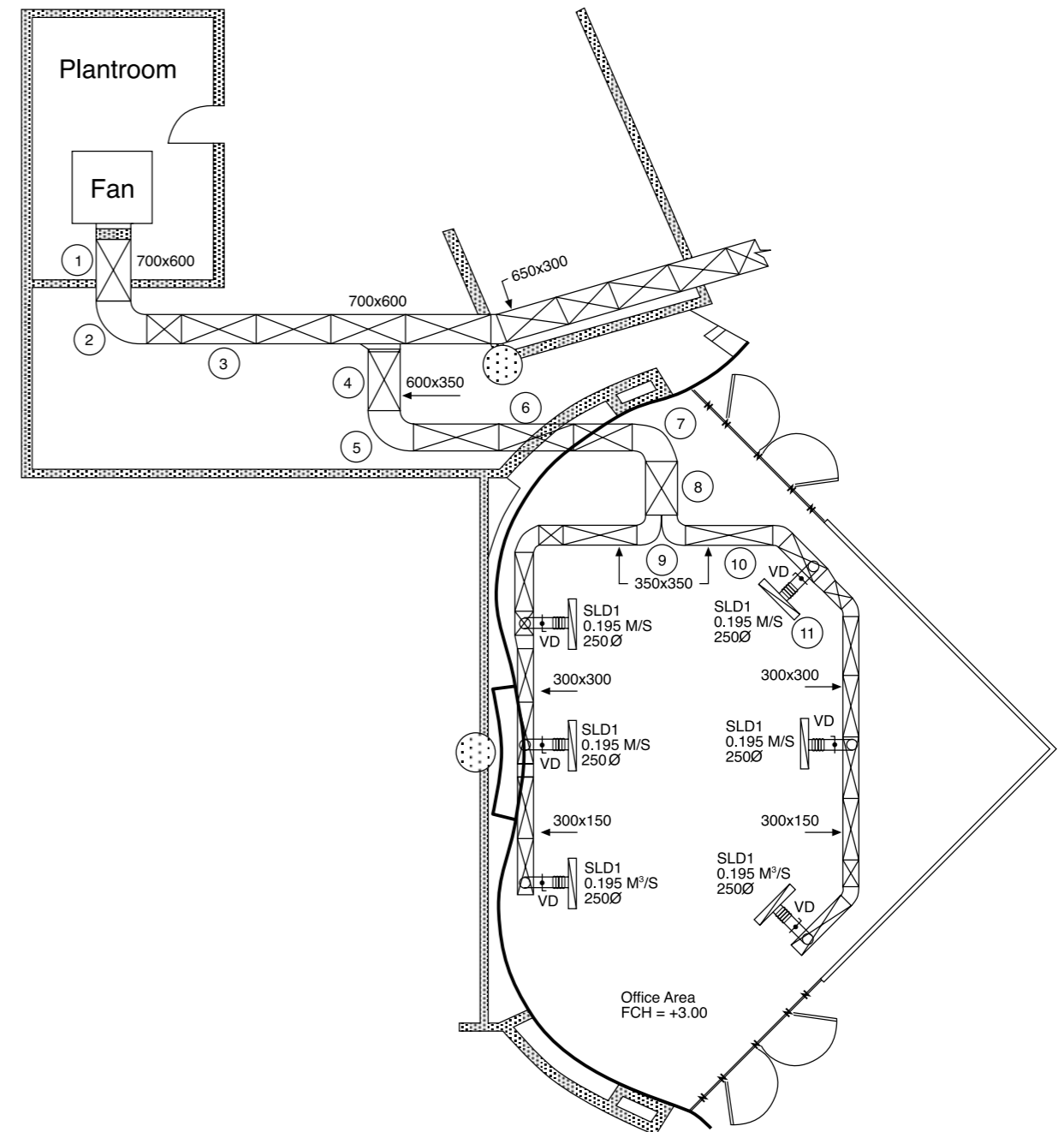
57	48	41	35	31	29	28	27
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<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>
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Octave Centre Frequency							
63	125	250	500	1k	2k	4k	8k

<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>
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Figure 1 : Duct System For Fan Noise Calculation Example



Calculation Example

The simple duct system shown in figure 1 will be entered on the calculation sheet to show the steps to be followed to determine whether sound attenuating materials are required to reduce the fan noise in a duct system.

For the duct system described in Figure 1, the sound power level produced by the fan is known from manufacturer's data. Calculate the sound pressure level in office area, at the nearest occupied position to a supply ceiling slot linear diffuser, which is given to be 1.5 meters from the diffuser and directly in line with its axis, and the diffusers are located in the ceiling.

Fan Details

Type : Centrifugal
 Duty : 2.26 m³/s at 600 Pa.
 Sound Power Level at mid frequency Octave Bands

Hz	63	125	250	500	1k	2k	4k	8k
dB	86	91	87	92	88	88	82	74

Room Details

Room Value : 300 m³
 Room Height : 3m
 Outlet : : Slot diffuser with 30mm neck width, 1200mm long. Slot diffuser handles 0.195 m³/s.

Room Criterion

NC 35 at 1.5 metres from the noise outlet.
 Office area

Roomside Calculation

System Element

Ref	Type	W	H	Length / Type
1	Duct	700	600	2 meters
2	Bend	700	600	Radiused
3	Duct	700	600	5 meters
4	Duct	600	350	2 meters
5	Bend	600	350	Radiused
6	Duct	600	350	6 meters
7	Bend	600	350	Radiused
8	Duct	600	350	2 meters
9	Bend	350	350	Radiused
10	Duct	350	350	2 meters
11	Outlet	2 slot diffuser, 30 mm neck width 1200 mm long		

Calculation Example

SAFID Acoustics

Project:
 Client:
 Contractor:
 Engineer:

Total Air Flow (M³/s) 2.26

Source Sound power Level

Smallest Ducts Dimension (mm)	600	Length (mm)	7
	350		12

Radiused Elbows Width (mm)	700	Qty.	1
	600		2
	350		1

Additional Attenuation	
------------------------	--

Outlet Reflection	Length (cm)	120	Width (cm)	3
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SWL Leaving System {a-(b+c)}

Percentage Leaving Outlet	M ³ /s	0.195	9%
Distance from Outlet to Listener (m)		1.5	
Directivity			Centre of Wall or Ceiling

Direct SPL {e-(f+g)+h}

Percentage Leaving Outlet	M ³ /s	1.17	52%	
Room Volume	Length x Width (m ²)	100	Height (m)	3
Reverberation Time			1 Second	

Reverberant SPL {e-(k+l)+m}

Combined SPL (logarithmic addition of i an o)

Criterion NC / NR / dBA	NC 35
Add dB Safety Factor	3

Required Insertion Loss

Sound Attenuator Selection

SA / O / 20 - 150 O / 900L x 700W x 600H
 Required Insertion Losses dB
 Selected Insertion Losses dB
 Attenuator Air Flow 2.26 M³/s
 Attenuator Pressure drop 47 Pa

Roomside Analysis Calculations

Date:
 Building:
 Equipment No:
 Offer No:

Octave Centre Frequency							
63	125	250	500	1k	2k	4k	8k
86	91	87	92	88	88	82	74
4.2	4.2	2.1	1.05	1.05	1.05	1.05	1.05
7.2	7.2	5.4	3.6	2.4	2.4	2.4	2.4
		1	2	3	3	3	3
		2	4	6	6	6	6
			1	2	3	3	3
15	10	6	2				
60	70	71	78	74	73	67	59
10	10	10	10	10	10	10	10
15	15	15	15	15	15	15	15
3	4	5	6	7	8	8	8
38	49	51	59	56	56	50	42
3	3	3	3	3	3	3	3
-11	-11	-11	-11	-11	-11	-11	-11
46	56	57	64	60	59	53	45
47	57	58	65	61	61	55	47
60	52	45	40	36	34	33	32
3	3	3	3	3	3	3	3
	8	16	28	28	30	25	18
Octave Centre Frequency							
63	125	250	500	1k	2k	4k	8k
8	14	20	37	47	32	26	24

General

SAFID attenuators were developed in response to various requirements from consulting engineers, owners and contractors. They provide the most economical choice for solving the wide range of noise control issues encountered in the HVAC field.

Our standard range of attenuators should cover most of the common problems in the HVAC industry, but if none of our standard silencers meet your requirements then we will develop one for your need.

Material

All SAFID attenuator are constructed of galvanized steel sheets as per ASTM A924 and ASTM A653 (replacing ASTM A525/A527).

Attenuators are also available in the following materials:

- Stainless steel as per ASTM 240 type 304 or 316.
- Epoxy coated (internally and externally).

Surface Finish

All SAFID galvanized attenuator are produced with G90 surface coating or 275g/m² zinc coating, regular spangle finish.

- All stainless steel attenuator are made with 2B mill finish.
- All epoxy coated attenuators are to be made to client requirements in terms of color and coating thickness.

Acoustic Infill

All SAFID "Acoustic Infill" material is inert, non-flammable, non-hygroscopic, will not sustain vermin or fungus, rot proof and odorless. The "Acoustic Infill" shall be faced with glass tissue or equivalent. The infill material is guaranteed against erosion up to air velocities of 30 m/s and temperatures up to 121°C.

The acoustic infill tested to the following tests:

- Surface Burning Characteristics: UL 723, ASTM E84, ASTM E136
- Mold Growth: ASTM D2020, UL 181
- Moisture Absorption: ASTM D-07 B, ASTM C550
- Fire Resistance: NFPA 90A
- Acoustic Performance: ASTM C1071, ASTM C423-77

Test Method

All SAFID attenuators are tested in accordance with BS 4718: 1971. "Methods of Test for silencers for Air Distribution Systems". These tests were carried out by the Sound Research Laboratories Limited in Sudbury, Suffolk, U.K.

The SRL Labs are equipped with the most up-to-date instruction and computer systems and able to conduct all acoustic and aerodynamic tests across the octave band frequency range 63Hz to 8KHz.

The laboratory measurement of insertion loss is defined as the arithmetic difference in the sound level of an electronically generated noise produced upstream of the test sample location with and without the test sample installed, when measured downstream of the test sample location.

The test ducting is assembled such that one end is located into a plenum containing the sound source and the outlet is fed into the 300 cubic metres reverberation room.

The static insertion loss is measured by placing a speaker in the duct and then measuring the noise levels in the test chamber with and without the attenuator. The difference between the measurements is calculated to give the insertion loss.

For the regenerated noise, measurements are made of the noise generated by air flowing through the duct system alone. Part of the duct work is then replaced by attenuator and the noise is measured again. The noise due to this system is then deducted from the noise measured with the attenuator to give the regenerated noise due solely to the attenuator.

From the above carried tests the insertion losses measurements have been recorded and derived and are presented in the tabular form in Table 17 of this section.



Description

The straight rectangular cased attenuator is mainly used to reduce fan and machine noise to meet the required or allowed noise levels. The SA attenuator offer many advanced features including as a standard aerodynamic splitters, side liners, slide on flange and protect acoustic infill by galvanized perforated sheet metal.

Construction

Type SA attenuator casings and splitters are manufactured from galvanized sheet metal Ga.20 minimum. Casing are formed with lock formed seams with a mastic sealant; the construction complies with SMACNA and DW 144 Standards. SAF - 30 slide on flanges are fitted as standard.

The splitters contain acoustic infill which complies with Class O Building Regulations. The infill has a glass tissue facing and is contained behind galvanized perforated metal; this dual protection prevents damage and fibre erosion up to 30 m/s airway velocity. The splitters are radiussed at both ends to minimize air pressure loss and regenerated noise.

Alternative Construction

SAHP

Type SAHP; as for type SA but with the casing thickness increased to Ga.18 to comply with ductwork codes SMACNA stds. high pressure & DW 144 Class C or D.

SAM

Type SAM; as for type SA but the acoustic infill is enveloped in a Melinex polyester film.

SAH

Type SAH; as for type SA but with horizontal splitters, normally to a maximum width dimension of 1200mm.

SAAF

Type SAAF; as for type SA but with rolled steel angle end flanges drilled to a standard pattern.

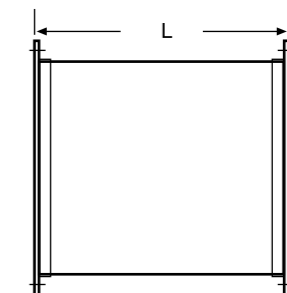
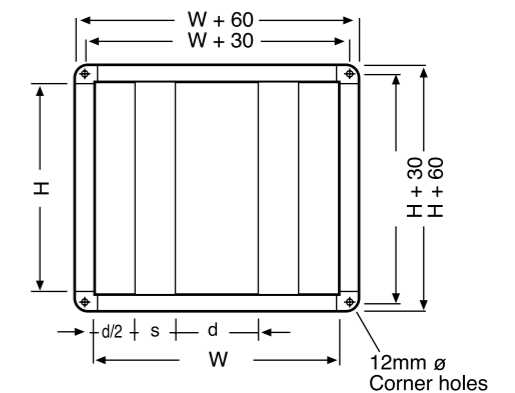
Sectionalised Construction

SA attenuators are normally supplied in sections when any of the following dimensions are exceeded: W=2100mm, H=1800mm, L=2100mm.

The assembly of sectionalised attenuators is on site, by others. SAFID will provide full details of attenuator configuration and assembly.

Dimensions

Attenuator: Type SA





SABV

Description

The vertical-mounted cased bend rectangular attenuator is mainly used to reduce fan and machine noise to meet the required or allowed noise levels. The SA attenuator offer many advanced features including as a standard aerodynamic splitters, side liners, slide on flange and protect acoustic infill by galvanized perforated sheet metal.

Construction

The construction of cased bend attenuators is generally as for the straight version. To minimize resistance to airflow, turning vanes are incorporated into the design.

Dimension L1 and L2 refer to the air entry and discharge legs respectively, measured along the center path of the bend until the intersection point so that $L_1 + L_2$ will be equal to L. Unless requested otherwise, bend attenuators would be supplied with L1 equal to L2.

Alternative Construction

SABVP
Type SABVP; as for type SABV but with the casing thickness increased to Ga.18 to comply with ductwork codes SMACNA stds. high pressure & DW 144 Class C or D.

SABVM
Type SAM; as for type SA but the acoustic infill is enveloped in a Melinex polyester film.

SABVF
Type SABVF; as for type SABV but with rolled steel angle end flanges drilled to a standard pattern.

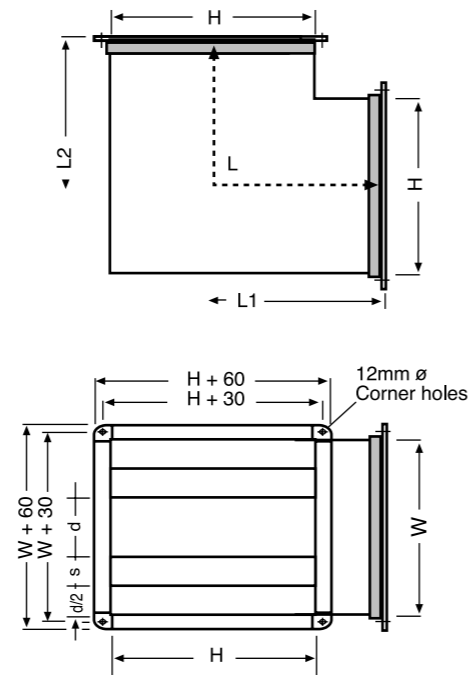
Sectionalised Construction

SABV attenuators are normally supplied in sections when any of the following dimensions are exceeded: W=2100mm, H=1800mm, L=2100mm

The assembly of sectionalised attenuators is on site, by others. SAFID will provide full details of attenuator configuration and assembly.

Dimensions

Vertical Bend Attenuator: Type SABV



SABH

Description

The horizontal-mounted cased bend rectangular attenuator is mainly used to reduce fan and machine noise to meet the required or allowed noise levels. The SA attenuator offer many advanced features including as a standard aerodynamic splitters, side liners, slide on flange and protect acoustic infill by galvanized perforated sheet metal.

Construction

The construction of cased bend attenuators is generally as for the straight version. To minimize resistance to airflow, turning vanes are incorporated into the design.

Dimension L1 and L2 refer to the air entry and discharge legs respectively, measured along the center path of the bend until the intersection point so that $L_1 + L_2$ will be equal to L. Unless requested otherwise, bend attenuators would be supplied with L1 equal to L2.

Alternative Construction

SABHP
Type SABHP; as for type SABH but with the casing thickness increased to Ga.18 to comply with ductwork codes SMACNA stds. high pressure & DW 144 Class C or D.

SABHM
Type SABHM; as for type SABH but the acoustic infill is enveloped in a Melinex polyester film.

SABHF
Type SABHF; as for type SABH but with rolled steel angle end flanges drilled to a standard pattern.

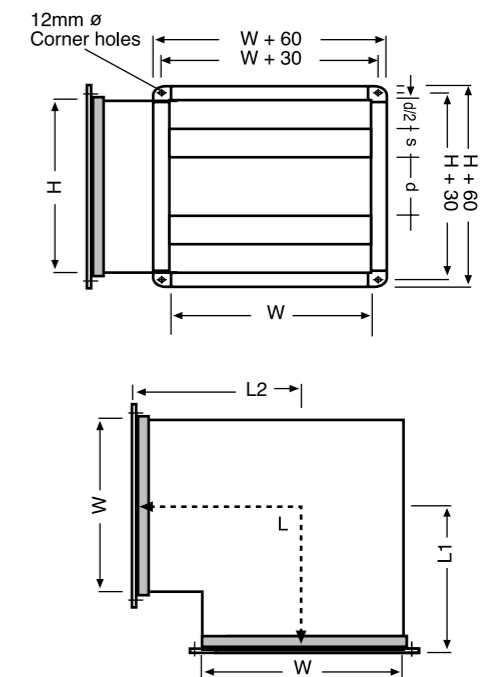
Sectionalised Construction

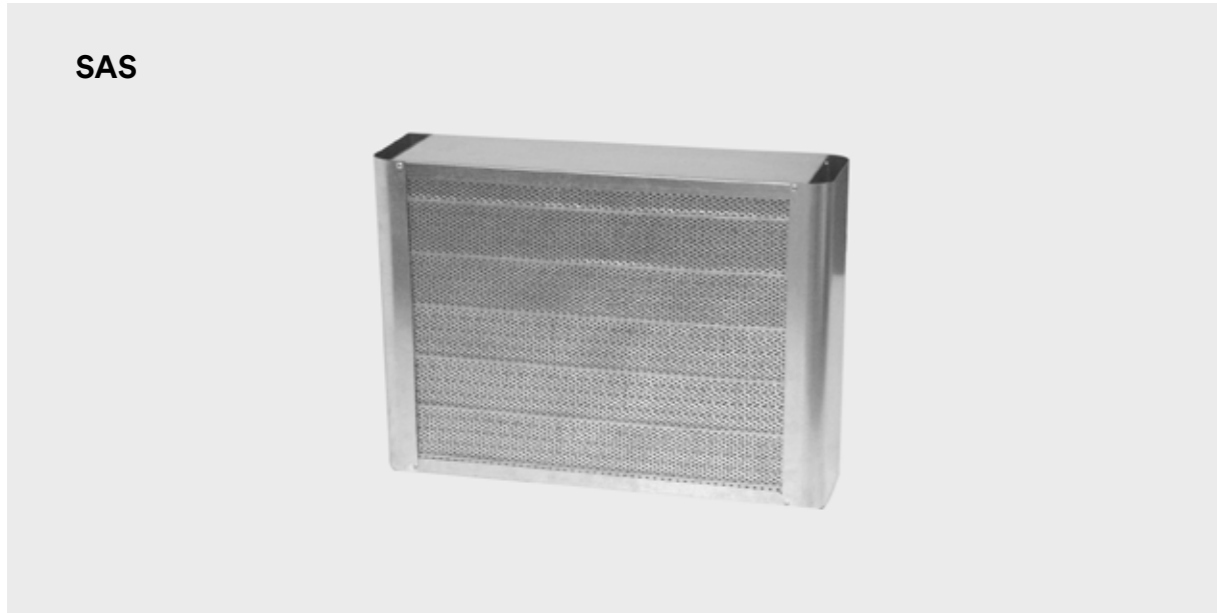
SABH attenuators are normally supplied in sections when any of the following dimensions are exceeded: W=2100mm, H=1800mm, L=2100mm

The assembly of sectionalised attenuators is on site, by others. SAFID will provide full details of attenuator configuration and assembly.

Dimensions

Horizontal Mounting Bend Attenuator: Type SABH





Description

The splitter or baffle are usually filled with acoustic infill, made to fit into builders work, ducts and shafts. It is designed for reducing fan noise, meeting specified Noise levels such as NC or NR.

Construction

Type SAS
Where preferred, Type SAS splitters only can be supplied for inclusion in an AHU section or builders work duct. Where required, airway spacer channels can be supplied.

The splitters contain acoustic infill which complies with Class O Building Regulations. The infill has a glass tissue facing and is contained behind perforated metal; this dual protection prevents damage and fibre erosion up to 30 m/s airway velocity. The splitters are radiused at both ends to minimize air pressure loss and regenerated noise.

A combination of acoustic splitter and airway produces an attenuator 'module'. The first 'module' comprises two half width side liners plus an airway.

Alternative Construction

SASM
Type SASM; as for type SAS but the acoustic infill is enveloped in a melinex polyester film.

Dimensions

Splitter Type SAS

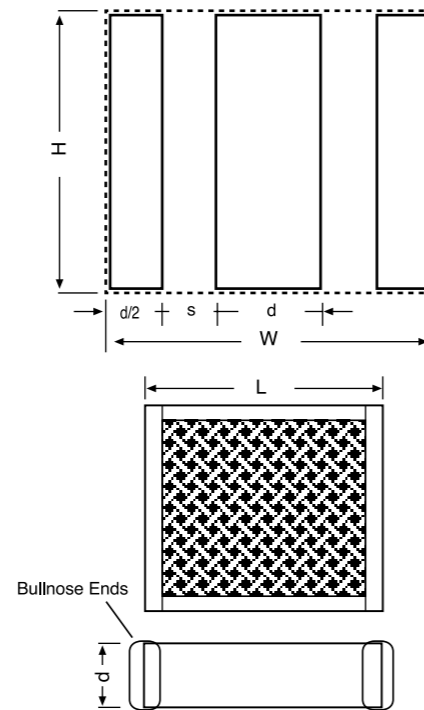


Table 1: Recommended design Criteria for Various Area Functions

Situation	NC
Section 1 - Studios and Auditoria	
Sound Broadcasting (drama)	15
Sound Broadcasting (general), TV (general), Recording Studio	20
TV (audience studio)	25
Concert Hall, Theatre	20 - 25
Lecture Theatre, Cinema	25 - 30
Section 2 - Hospitals	
Audiometric Room	20 - 25
Operating Theatre, Single Bed Ward	30 - 35
Multi-bed Ward, Waiting room	35
Corridor, Laboratory	35 - 40
Wash Room, Toilet, Kitchen	35 - 45
Staff Room, Recreation Room	30 - 40
Section 3 - Hotels	
Individual Room, Suite	20 - 30
Ballroom, Banquet Room	30 - 35
Corridor, Lobby	35 - 40
Kitchen, Laundry	40 - 45
Section 4 - Restaurants, Shops and Stores	
Restaurant, Department Store (upper floor)	35 - 40
Club, Public House, Cafeteria, Canteen, Retail Store (main floor)	40 - 45
Section 5 - Offices	
Boardroom, Large Conference Room	25 - 30
Small Conference Room, Executive Office, Reception Room	30 - 35
Open Plan Office	35
Drawing Office, Computer Suite	35 - 45
Section 6 - Public Buildings	
Court Room	25 - 30
Assembly Hall	25 - 35
Library, Bank, Museum	30 - 35
Wash Room, Toilet	35 - 45
Swimming Pool, Sports Arena	40 - 45
Garage, Car Park	55
Section 7 - Ecclesiastical and Academic Buildings	
Church, Mosque	25 - 30
Classroom, Lecture Theatre	25 - 35
Laboratory, Workshop	35 - 40
Corridor, Gymnasium	35 - 45
Section 8 - Industrial	
Warehouse, Garage	45 - 50
Workshop (light engineering)	45 - 55
Workshop (heavy engineering)	50 - 65
Section 9 - Private Dwelling (Urban)	
Bedroom	25
Living Room	30

ATTENUATOR PERFORMANCE



SA attenuator have been rated, tested and derived from tests meeting the requirements of BS 4718: 1971 as tests conducted by SRL of UK.

No deviations of insertion loss with airflow were recorded over the range of velocities employed in this catalogue. Static insertion loss figures are provided in Table 3.

Full regenerated noise data is available for SA attenuators to enable installed insertion loss to be calculated. Table 2 gives guidelines for maximum face velocity against design noise level requirements, in order to limit attenuator regenerated noise.

Pressure loss data assumes that the airflow to the attenuator is uniform over the face, in a duct-to-duct layout. Units installed in situations leading to poor inlet or discharge conditions could incur pressure losses higher than catalogued.

In most applications the requirement to keep the pressure drop across the attenuator to a reasonable level automatically ensures that the flow noise generated within the attenuator is insignificant compared with the permissible sound power which emerges. If however, extremely low levels have to be obtained, or if the sound power from the fan is relatively low, the flow noise generated by the attenuator can be significant and can reduce its effective insertion loss. It is for this reason that when an acoustic consultant specifies the attenuator performance he will normally specify the insertion loss which is required. This then enables the attenuator manufacturer to select a unit of such a size that the flow generated within it will not reduce the effective insertion loss below the required level.

Assuming correct installation, acoustic and aerodynamic performance of splitters only will be as for a cased attenuator.

Description

Space noise levels can be affected by attenuator self noise. As a guide it is recommended that the face velocities indicated are not exceeded. For systems with fewer than three outlets or less than 5m of ductwork, size for 5NC lower. For design levels of NC30 or below the selection should be checked by SAFID.

Table 2: Installed Insertion Loss (Velocity)

Required Space Noise Level (NC)	Face Velocity (v, m/s)			
	Attenuator Type			
	SA 20 - 75	SA 20 - 100	SA 20 - 150	SA 20 - 200
25	2.4	3.2	3.9	5.0
30	3.2	4.2	5.5	6.2
35	3.8	5.0	6.7	7.4
40	4.6	5.7	7.7	8.9
45	5.4	6.6	8.6	10.4
50	6.2	7.6	9.7	11.6



ATTENUATOR PERFORMANCE

Table 3: Static Insertion Loss (dB)

SA 20 - 75 Attenuators		Octave Centre Frequency (f _m in Hz)							
Type	Length (mm)	63	125	250	500	1k	2k	4k	8k
SA 20 - 75	600	9	13	22	36	45	39	33	29
SA 20 - 75	900	10	16	27	41	49	47	38	33
SA 20 - 75	1200	11	18	31	46	50	50	43	38
SA 20 - 75	1500	12	21	36	50	50	50	48	42
SA 20 - 75	1800	13	24	41	50	50	50	50	46
SA 20 - 75	2100	14	26	45	50	50	50	50	50
SA 20 - 75	2400	15	29	50	50	50	50	50	50
SA 20 - 100 Attenuators		Octave Centre Frequency (f _m in Hz)							
Type	Length (mm)	63	125	250	500	1k	2k	4k	8k
SA 20 - 100	600	7	10	18	34	46	40	33	29
SA 20 - 100	900	8	12	22	37	50	46	36	31
SA 20 - 100	1200	9	14	26	40	50	50	39	33
SA 20 - 100	1500	9	17	30	44	50	50	41	35
SA 20 - 100	1800	10	19	34	47	50	50	44	37
SA 20 - 100	2100	11	21	38	50	50	50	47	39
SA 20 - 100	2400	11	24	42	50	50	50	49	41
SA 20 - 150 Attenuators		Octave Centre Frequency (f _m in Hz)							
Type	Length (mm)	63	125	250	500	1k	2k	4k	8k
SA 20 - 150	600	8	12	17	34	44	28	23	22
SA 20 - 150	900	8	14	20	37	47	32	26	24
SA 20 - 150	1200	9	15	23	40	50	36	29	26
SA 20 - 150	1500	10	17	26	43	53	40	32	28
SA 20 - 150	1800	11	18	29	46	57	44	35	31
SA 20 - 150	2100	11	20	32	49	40	48	38	33
SA 20 - 150	2400	12	21	35	50	50	50	41	35
SA 20 - 200 Attenuators		Octave Centre Frequency (f _m in Hz)							
Type	Length (mm)	63	125	250	500	1k	2k	4k	8k
SA 20 - 200	600	7	11	16	25	27	23	21	20
SA 20 - 200	900	8	12	18	30	33	26	23	21
SA 20 - 200	1200	8	14	21	35	39	30	25	23
SA 20 - 200	1500	9	15	23	40	44	33	28	24
SA 20 - 200	1800	9	17	26	45	50	37	30	26
SA 20 - 200	2100	10	18	28	50	50	40	32	27
SA 20 - 200	2400	11	19	30	50	50	43	34	28

Quick Selection

The SAFID leaflet titled "Sound and Noise Control" and other technical sources, describe the method for full acoustic analysis. If attenuator performance requirements have been established in this way, then reference should be made to Table 3.

However, to enable engineers to produce attenuator selections to assist in design planning, Table 4 has been devised. It is recommended that SAFID engineers check the attenuators selections, when detailed system data is available.

Requirements for noise levels of NC30 or below should be referred to SAFID for analysis.

Larger and alternative cross section can be selected from Tables 5 to 8. Note that the width dimension (Type SA) or height dimension (Type SAH) must be in a 'modular' increment. Air pressure loss can be taken from the tables for the appropriate face velocity.

For Atmosphere side noise assessment consult SAFID.

Method of Selection

- 1 From Table 1 select the recommended space NC level for the type of area concerned.
- 2 From Table 4 select an attenuator for appropriate fan static pressure, type of ventilated space and space NC level.
- 3 From Table 2 check for maximum attenuator face velocity permissible for space NC level required.
- 4 From Table 5 to 8 as applicable, select a cross section for the attenuator for the volume flow rate required and to satisfy the maximum desirable face velocity / pressure loss.
- 5 Selection example:
SA20-150 / 700W x 600H x 1500L

Table 4: Attenuator Quick Selection Chart

		Type of ventilated area being served by low velocity systems utilizing DW 142 Classes A or B ductwork									High velocity CV/ VAV systems incorporating terminal units and utilizing DW 142 Class C ductwork.
		Rooms with average furnishing: floors carpeted, including:			Rooms with limited furnishings: mainly hard surfaces, including:			Rooms without soft furnishings, including:			
		Offices, Banks, Libraries, Lecture rooms, Restaurants Hotel rooms, Department stores.			Hospital areas, Supermarkets, Computer rooms, Clean rooms, Laboratories, Cafes, Dance Halls, Museums, Canteens, Toilets.			Kitchens, Swimming Pools, Sports Halls, Covered garages, Warehouses.			
Fan Static Pressure	Criterion Type	250 Pa	500 Pa	1000 Pa	250 Pa	500 Pa	1000 Pa	250 Pa	500 Pa	1000 Pa	2000 Pa Max
		Attenuator Length (mm)			Attenuator Length (mm)			Attenuator Length (mm)			Attenuator Length (mm)
NC 45	SA20-100	900	900	900	900	900	1200	900	900	1500	1200
	SA20-150	900	1200	1200	1200	1500	1800	1500	900	2100	1800
NC 40	SA20-100	900	900	1200	1200	1200	1500	1200	1500	1500	1500
	SA20-150	1200	1500	1800	1500	1800	2100	1800	2100	2100	2100
NC 35	SA20-100	1200	1200	1500	1500	1500	1800	1500	1800	1800	1800
	SA20-150	1500	1800	2100	1800	2100	1400	1800	2100	2400	2400

FULL METHOD

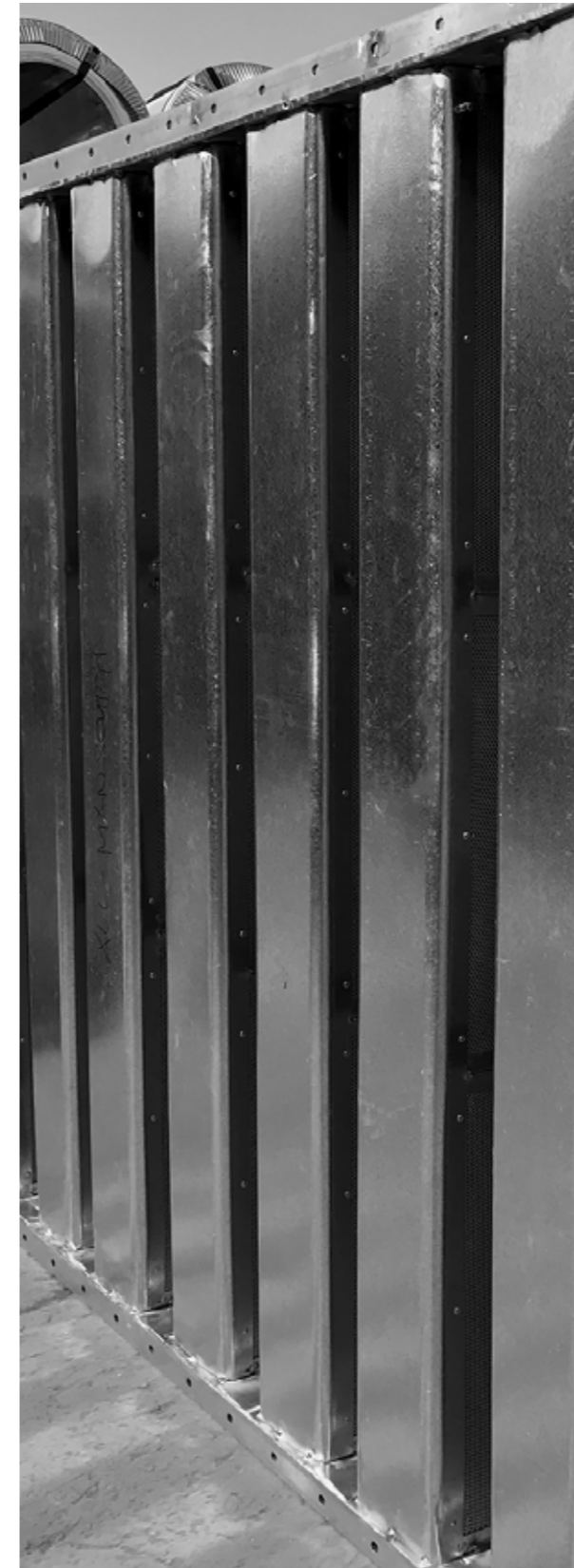
Full Selection

When an attenuator performance requirement has been established, for example, after following the procedure in the Safid "Sound & Noise Control" brochure, a suitable SA attenuator can be selected from the following Method of Selection. If the acoustic performance is not known, then a selection can be obtained using the Quick Selection Method on page 46.

Larger and alternative cross sections can be selected from Tables 5 to 8. Note that the width dimension (Type SA) or height dimension (Type SAH) must be in a 'modular' increment. Air pressure loss can be taken from the tables for the appropriate face velocity.

Method of Selection

- 1 From Table 3 select an attenuator to meet the performance needs.
- 2 From Table 2 check for maximum attenuator face velocity permissible for space NC level required.
- 3 From Table 5 to 8 as applicable, select an attenuator cross-section for the required volume flow rate and to satisfy the maximum desirable face velocity / pressure loss.
- 4 Selection example:
SA20-100 / 600W x 600H x 1200L



NOTE

The data below should not be used where Melinex (polyester membrane) faced attenuators are required, since the use of the membrane modifies acoustic performance. Performance requirements higher than shown in Table 3 should be referred to SAFID for selection.

Weight SA20 Cased Attenuator

Width (mm)	SA20-75	275	550	825	1100	1325	1650	1925
	SA20-100	300	600	900	1200	1500	1800	2100
	SA20-150	350	700	1050	1400	1750	2100	-
	SA20-200	400	800	1200	1600	2000	-	-
Number of Modules	1	2	3	4	5	6	7	
Length 'L' (mm)	Height 'H' (mm)	Weight (kg ± 10%)						
600	300	16	26	36	46	56	64	70
	600	23	36	49	62	75	87	95
	900	30	46	62	78	94	110	120
	1200	37	56	75	93	113	132	145
	1500	-	66	82	110	131	153	169
1800	-	-	106	132	159	185	205	
900	300	22	36	49	63	77	90	98
	600	31	49	66	84	102	119	130
	900	41	63	84	106	128	150	164
	1200	50	76	101	127	153	179	197
	1500	-	90	116	148	178	207	229
1800	-	-	144	180	216	252	280	
1200	300	26	44	61	79	97	115	123
	600	38	60	82	104	127	149	162
	900	50	78	106	133	161	189	207
	1200	63	95	127	160	192	225	248
	1500	-	113	149	186	224	261	289
1800	-	-	182	227	273	319	355	
1500	300	30	51	72	92	113	134	144
	600	44	70	96	121	147	173	188
	900	58	90	122	154	186	218	239
	1200	72	110	147	185	222	259	286
	1500	-	130	172	215	258	301	333
1800	-	-	210	262	315	368	409	
1800	300	42	70	95	122	150	176	193
	600	60	96	130	165	201	235	256
	900	80	124	166	208	252	297	325
	1200	98	150	199	250	301	355	390
	1500	-	178	230	293	351	411	454
1800	-	-	284	355	427	500	554	
2100	300	46	78	108	140	172	203	219
	600	67	107	146	186	227	265	290
	900	89	138	187	236	286	335	365
	1200	110	167	225	284	340	400	440
	1500	-	200	261	330	398	464	513
1800	-	-	322	401	485	565	629	

Weight SAS Splitters Only

Width in Modules		One Module	Each Additional Modules
Length 'L' (mm)	Height 'H' (mm)	Weight (kg ± 10%)	
600	300	6	5
	600	10	8
	900	14	10
	1200	17	13
	1500	20	15
1800	27	17	
900	300	9	7
	600	14	10
	900	20	14
	1200	25	18
	1500	30	21
1800	39	25	
1200	300	11	8
	600	17	13
	900	25	18
	1200	34	23
	1500	42	27
1800	55	31	
1500	300	13	10
	600	21	16
	900	30	22
	1200	34	28
	1500	51	32
1800	66	38	
1800	300	17	11
	600	28	19
	900	39	25
	1200	55	32
	1500	66	37
1800	78	45	
2100	300	19	13
	600	30	19
	900	44	28
	1200	61	35
	1500	75	44
1800	88	52	

NOTE:
The data below should not be used where Melinex (polyester membrane) faced attenuators are required, since the use of the membrane modifies acoustic performance. Performance requirements higher than shown in Table 3 should be referred to SAFID for selection.

W = 2100mm H = 1800mm L = 2100mm

Nomenclature:

- W in mm : Width inside duct.
- H in mm : Height in duct.
- L in mm : Length
- d in cm : Splitter thickness
- s in mm : Airway width.
- V in l/s : Volume flow rate.
- v_f in m/s : Face velocity based on V ÷ (W x H x 1000).
- Δp in Pa : Pressure loss.
- f_m in Hz : Octave centre frequency.
- d_e in dB : Insertion loss.
- NC in dB : Noise criterion

Order Details

Order Code for Cased Attenuator SA / M / 20-100 / EP / 1800 x 1200 x 900

Attenuator Type _____

Type Suffix:

O: Standard _____

H: Horizontal Airways _____

HP: High Pressure Casing _____

M: Melinex infill wrap _____

BV: Bend Vertical _____

BH: Bend Horizontal _____

AF: Angle Flange Connections _____

X: Evase Tail _____

U: Without perforated sheet _____

Splitter thickness in cm _____

Airways in mm _____

Material Finish:

O: Standard _____

SS-304: Stainless Steel Grade 304 _____

SS-316: Stainless Steel Grade 316 _____

EP: Epoxy Painted (both surfaces) _____

EPI: As above, internal surfaces only _____

EPE: As above, external surfaces only _____

Order Code for Splitter SAS / M / 20-100 / EP / 1800 x 1200 x 900

Attenuator Type _____

Type Suffix:

O: Standard _____

H: Horizontal Airways _____

M: Melinex infill wrap _____

Splitter thickness in cm _____

Airways in mm _____

Material Finish:

O: Standard _____

SS-304: Stainless Steel Grade 304 _____

SS-316: Stainless Steel Grade 316 _____

EP: Epoxy Painted (both surfaces) _____

Specifications

Cased Attenuators

Type SA splitter attenuator, incorporating aerodynamic splitters and side liners with erosion protected Class O acoustic infill covered by perforated sheet metal. Casing construction conforms with SMACNA & DW 144 Standards. Flange connections are SAF -30 or SAF - 35 slide on type.

Splitters Only

Type SAS splitters only, for installation in ductwork by others, featuring aerodynamic leading and trailing edges with erosion protected Class O acoustic infill covered by galvanized perforated sheet metal. The splitter frame is manufactured from Ga.20 galvanized sheet metal.

Order Example

Standard For Sound Attenuator

Make : SAFID

Type : SA20-100 / 1800 × 1200 × 900

Qty : 1

Standard For Splitter

Make : SAFID

Type : SAS20-100 / 1800 × 1200 × 900

Qty : 1



INTRODUCTION TO CYNDRICAL SOUND ATTENUATORS

Introduction

For many years noise was something to be tolerated. Unpleasant perhaps, but no more than that.

While it has been recognised for many years that the exposure of work-people to noise is hazardous and that noise-induced hearing loss cannot be corrected to any significant degree by means of medical treatment. The cost of ignoring noise is the impaired hearing of factory workers, an inability to work properly under almost unbearable sound levels, and a whole variety of social effects.

In schools, offices, hospitals, noise can interfere with communication and disrupts concentration.

In any building project where consideration is given to the internal or external acoustic environments, it is necessary to formulate certain targets at the preliminary planning stages in order that desired comfort conditions are attained.

Mechanical equipment noise is one of the major sources of unwanted noise in a building. The primary considerations given to the selection and use of mechanical equipment in buildings have generally been only those directly related to the intended use of the equipment. However, with the trend towards light weight building structures and variable-volume air distribution systems, the noise generated by mechanical equipment and the design of equipment spaces should not only be undertaken with an emphasis on the intended uses of the equipment, but also with a desire to provide acceptable noise levels in the occupied spaces of the building in which the equipment is located.

Test Method

All SAFID attenuators are tested in accordance with BS 4718 : 1971.

The laboratory measurement of insertion loss is defined as the arithmetic difference in the sound level of an electronically generated noise produced upstream of the test sample location with and without the test sample installed, when measured downstream of the test sample location.

The test ducting is assembled such that one end is located into a plenum containing the sound source and the outlet is fed into the 300 cubic metres reverberation room.

Static insertion loss is measured by placing a speaker in the duct and then measuring the noise levels in the test chamber with and without the attenuator. The difference between the measurements is calculated to give the insertion loss.

For the regenerated noise, measurements are made of the noise generated by air flowing through the duct system alone. Part of the duct work is then replaced by attenuator and the noise is measured again. The noise due to this system is then deducted from the noise measured with the attenuator to give the regenerated noise due solely to the attenuator.



Description

The cylindrical attenuators are prefabricated sections of double wall ductwork with solid outer shell and perforated inner shell. The space between the two shells are usually filled with acoustic infill. It is designed for reducing fan noise, meeting specified noise levels such as NC or NR.

Construction

Type SAC attenuators are available in a size range based upon ISO standards. Two lengths are catalogued, nominally equivalent to one times inside duct diameter with increased lengths available where higher acoustic performance is required. Alternative sizes and end connection types can be provided.

Standard attenuator casings are manufactured from galvanized sheet metal Ga.20 minimum. Casings are constructed with grooved seams with a mastic sealant; casing thickness complies with SMACNA standards and DW 144 Class B ductwork code. End plates contain threaded inserts M6-M10 as standard depending upon attenuator size. The attenuators contain acoustic infill has a glass cloth facing and is contained behind galvanized perforated sheet metal; this dual protection prevents damage and fibre erosion up to 30 m/s airway velocity.

Alternative Construction

SACH
Type SACH; as for type SAC but with the casing thickness increased to comply with ductwork codes SMACNA standards - high pressure and DW 144 Class C or D.

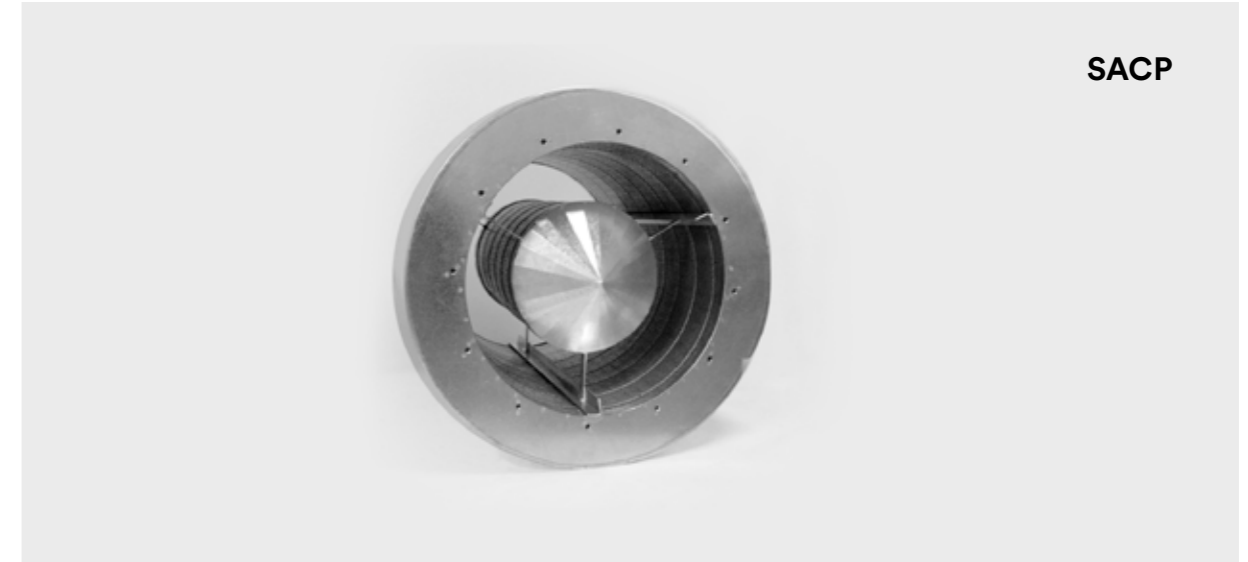
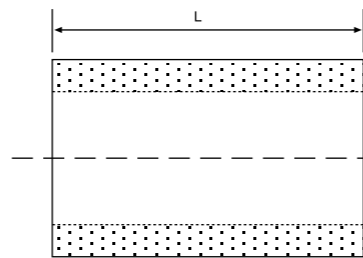
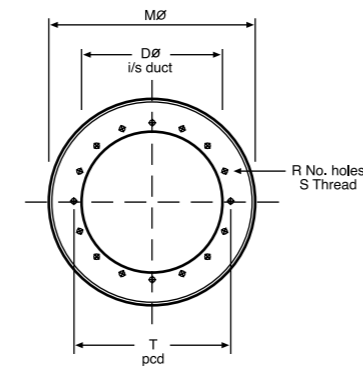
SACM
Type SACM; as for type SAC but the acoustic infill is enveloped in a Melinex polyester film.

Sectionalised Construction

Attenuators would normally be supplied split on length when the "L" dimension exceeds 2000mm, for site assembly by others. Coupling angles are supplied.

The assembly of sectionalised attenuators is on site, by others. SAFID will provide full details of attenuator configuration and assembly.

Dimensions



Description

The podded cylindrical attenuators are prefabricated sections of double wall ductwork with solid outer shell, perforated inner shell and incorporates an aerodynamically efficient concentric pod. The space between the two shells and pod are usually filled with acoustic infill. It is designed for reducing fan noise, meeting specified noise levels such as NC or NR.

Construction

Type SACP attenuators are available in a size range based upon ISO standards. Two lengths are catalogued, nominally equivalent to one times inside duct diameter with increased lengths available where higher acoustic performance is required. Alternative sizes and end connection types can be provided.

Standard attenuator casings are manufactured from galvanized sheet metal Ga.20 minimum. Casings are constructed with grooved seams with a mastic sealant; casing thickness complies with SMACNA standards and DW 144 Class B ductwork code. End plates contain threaded inserts M6-M10 as standard depending upon attenuator size. The attenuators contain acoustic infill has a glass cloth facing and is contained behind galvanized perforated sheet metal; this dual protection prevents damage and fibre erosion up to 30 m/s airway velocity.

Alternative Construction

SACPH
Type SACPH; as for type SACP but with the casing thickness increased to comply with ductwork codes SMACNA standards - high pressure and DW 144 Class C or D.

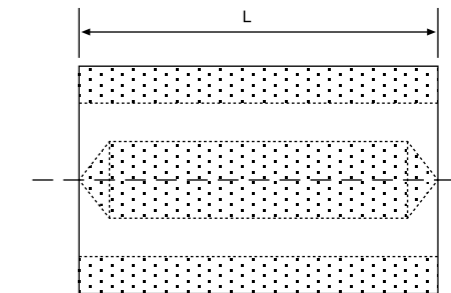
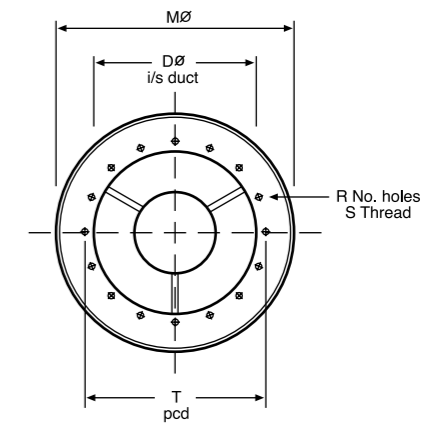
SACPM
Type SACPM; as fo type SAC but the acoustic infill is enveloped in a Melinex polyester film.

Sectionalised Construction

Attenuators would normally be supplied split on length when the "L" dimension exceeds 2000mm, for site assembly by others. Coupling angles are supplied.

The assembly of sectionalised attenuators is on site, by others. SAFID will provide full details of attenuator configuration and assembly.

Dimensions



ATTENUATOR SELECTION



Acoustic Performance

Performance

Attenuator performance is derived from tests meeting the requirements of BS 4718 : 1971.

Cylindrical attenuators follow a similar principle, however, in this case the splitter consisting of a pod in the middle of a lined cylindrical duct.

Attenuator selection is based on the static insertion loss performance, the aerodynamic resistance or pressure drop, and the regenerated sound power levels. Static insertion loss figures are given in the table.

Full regenerated noise data is available for SAFID cylindrical attenuators, to enable installed Insertion Loss to be calculated.

Pressure loss data relates to pod type attenuators and assumes that the airflow to the attenuator is uniform over the face, in a duct to duct layout. Units installed in situations leading to poor inlet or discharge conditions could incur pressure drops higher than catalogued. Podless attenuators have a pressure loss similar to an equivalent length of ductwork.

For insertion loss data for Melinex faced attenuators - refer to SAFID.

Nomenclature

L in mm : Length

D in mm : Inside diameter

V in l/s : Volume flow rate

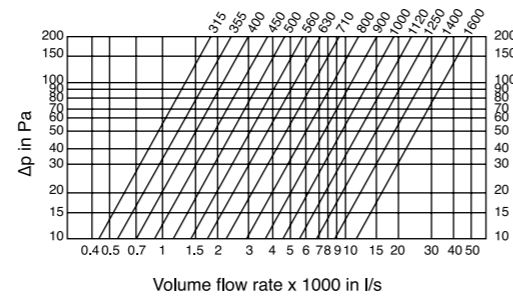
Δp in Pa : Pressure loss

f_m in Hz : Octave centre frequency

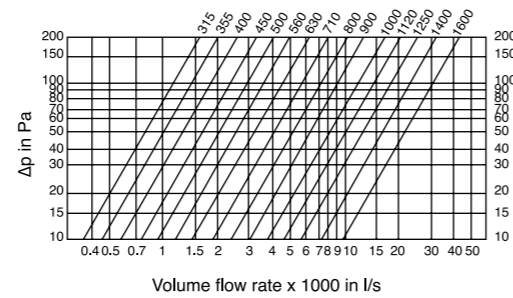
D_s in dB : Insertion loss

Pressure Loss

Pressure loss for type SACP-1D



Pressure loss for type SACP-2D



ATTENUATOR PERFORMANCE

Acoustic Performance

Attenuator		Insertion Loss (dB)							
		Octave Centre Frequency (Hz)							
Size	Type	63	125	250	500	1000	2000	4000	8000
250	SAC-1D	2	3	6	11	12	7	6	4
	SAC-2D	4	5	10	21	22	13	10	8
315	SAC1-D	2	3	6	12	11	7	6	4
355	SAC2-D	4	5	10	21	22	13	10	8
400									
450	SACP-1D	5	6	10	16	22	24	20	15
	SACP-2D	9	12	18	30	44	48	38	29
500	SAC-1D	2	3	6	11	12	7	6	4
560	SAC-2D	4	5	10	21	20	10	9	6
630									
710	SACP-1D	5	6	10	16	22	23	17	12
800									
900	SACP-2D	9	12	18	30	44	45	33	24
	1000	SAC-1D	2	3	6	11	8	5	4
1120	SAC-2D	4	5	10	21	16	9	8	5
1250									
1400	SACP-1D	5	6	10	16	22	22	15	11
1600									
	SACP-2D	9	12	18	30	44	42	29	21

Weights

Unit	Dimensions (End Plate for Flange Connection)							Weights (kg)			
	D	M	L	L	T	R	S	SAC	SAC	SACP	SACP
Size	f	f	1D	2D	pcd	No. of Holes	Thread Size	1D	2D	1D	2D
250	256	456	250	500	286	6	M6	9	13	-	-
315	322	522	300	600	356	8	M8	11	15	14	20
355	361	561	350	700	395	8	M8	15	21	20	28
400	404	604	400	800	438	12	M8	18	27	26	36
450	453	653	450	900	487	12	M8	24	35	34	42
500	507	707	500	1000	541	12	M8	29	41	41	57
560	564	764	550	1100	605	16	M10	35	50	50	70
630	638	838	600	1200	674	16	M10	42	58	58	82
710	715	915	700	1400	751	16	M10	51	72	72	100
800	801	1001	800	1600	837	24	M10	58	82	79	111
900	898	1098	900	1800	934	24	M10	70	100	97	135
1000	1007	1207	1000	2000	1043	24	M10	95	135	120	185
1120	1130	1330	1100	2200	1174	24	M10	115	160	145	215
1250	1267	1467	1250	2500	1311	24	M10	130	180	165	240
1400	1421	1622	1400	2800	1465	24	M10	210	420	270	520
1600	1593	1793	1600	3200	1637	32	M10	250	490	320	620

Order Details

Order Code	SAC / 2D / 630 / H / SS-304
Attenuator Type:	
SAC without pod	_____
SACP with Pod	_____
Attenuator Length:	
1D; nominally 1 times diameter	_____
2D; nominally 2 times diameter	_____
Attenuator Size	_____
Construction:	
O: Standard	_____
H: High Pressure Casing	_____
M: Melinex Infill Wrap	_____
Material Finish:	
O: Standard	_____
SS-304: Stainless Steel Grade 304	_____
SS-316: Stainless Steel Grade 316	_____
EP: Epoxy Painted (both surfaces)	_____
EPI: As above, internal surfaces only	_____
EPE: As above, external surfaces only	_____
GAM: manufacture casing and perforated facing	_____

Specification Text

Type SAC/SACP cylindrical attenuators incorporating erosion protected Class O acoustic infill covered by perforated sheet metal. The casing is manufactured to DW 144 Class B medium pressure construction from galvanized sheel metal of the appropriate thickness. End plates fitted with threaded nut inserts.

Order Example

Make : SAFID
 Type : SAC-2D/630/HP/SS-304
 Qty : 1

Introduction

The fan is not the only source of airborne sound power which can be transmitted through ductworks. Just as sound power can come out of ducts through air devices in rooms, it can also enter these openings. If two rooms are served by branches on a common duct system or if walls or partitions has air transfer openings, the greater possibility of sound to transmit from one room to adjoining room. Sound in one room which can be transmitted to adjoining room may came from many sources such as raised voice, office equipments or machinery. This sound path is called crosstalk. A suitable method of preventing or reducing crosstalk to attain the required room noise level is by installing crosstalk attenuator.

Application

The crosstalk attenuators are commonly used to prevent noise transmission via common ceiling, duct system or in air transfer openings on walls or partitions between adjoining rooms.

These units are designed and built for optimum noise control in a situation where the noise in the first room is clearly heard in the second room.





Description

The crosstalk attenuators are prefabricated sections of ductwork with acoustic lining.

It is designed to avoid noise radiated from a room or from a duct termination which is connected via a main duct, to a branch duct leading to another room. Airflow is permitted whilst noise transfer is limited.

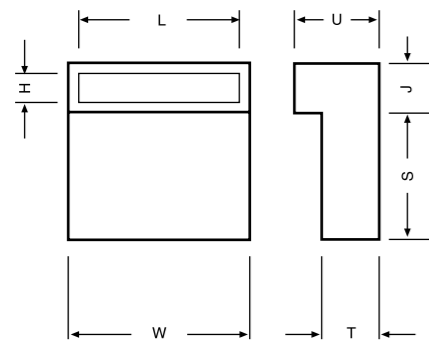
Construction

Type SCTL attenuators have been designed to avoid noise interference between interconnected rooms. It is used as air transfer attenuators between adjoining areas where the acoustic integrity of a common partition or ceiling needs to be maintained.

Casing are manufactured from galvanized sheet metal Ga.20, with spot welded seams. The acoustic lining complies with Class O Building Regulations and has a glass tissue facing for erosion protection. The units may be supplied with one or two eggcrated grilles in natural anodised aluminium. Colour paint finishes are available to order.

Dimensions

Type SCTL

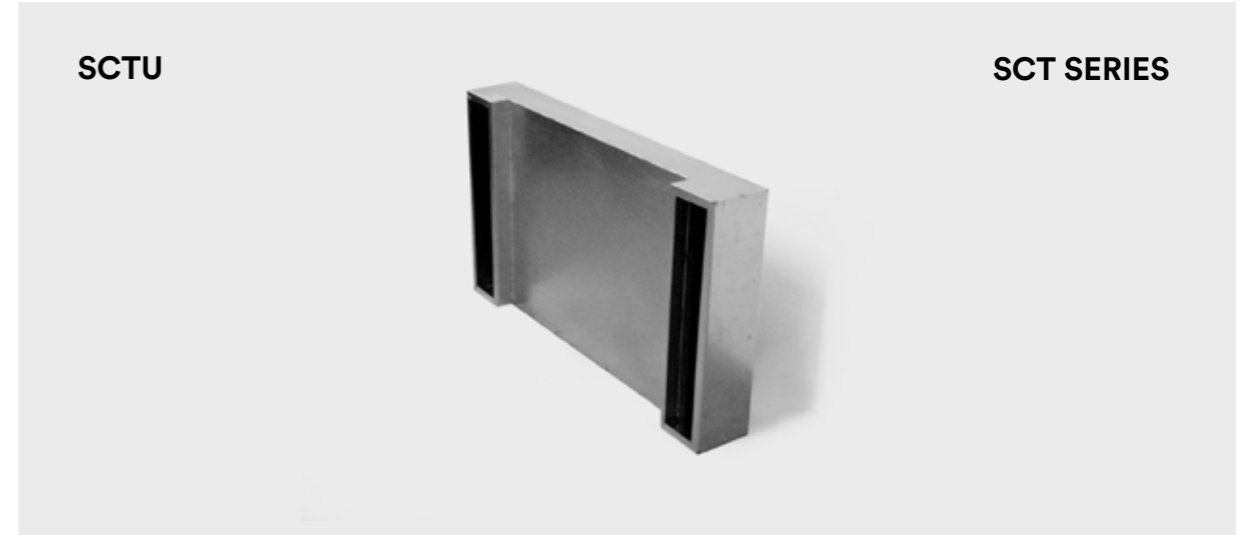
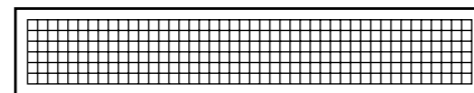


Standard Sizes

Unit Size	H	L	J	W	T	U	S
1	100	550	140	590	100	120	760
2	100	700	140	740	100	120	760
3	100	900	140	940	100	120	760
4	100	1000	140	1040	100	120	760
5	100	1200	140	1240	100	120	760

Optional Grilles: Eggcrate Pattern

Standard Supply: For Type SCTL One no.



Description

The crosstalk attenuators are prefabricated sections of ductwork with acoustic lining.

It is designed to avoid noise radiated from a room or from a duct termination which is connected via a main duct, to a branch duct leading to another room. Airflow is permitted whilst noise transfer is limited.

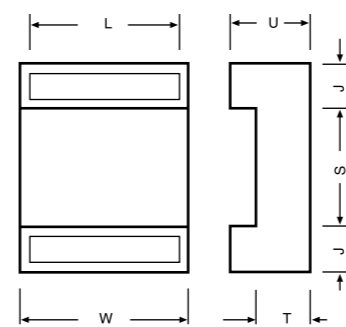
Construction

Type SCTU attenuators have been designed to avoid noise interference between interconnected rooms. It is used as air transfer attenuators between adjoining areas where the acoustic integrity of a common partition or ceiling needs to be maintained.

Casing are manufactured from galvanized sheet metal Ga.20, with spot welded seams. The acoustic lining complies with Class O Building Regulations and has a glass tissue facing for erosion protection. The units may be supplied with one or two eggcrated grilles in natural anodised aluminium. Colour paint finishes are available to order.

Dimensions

Type SCTU

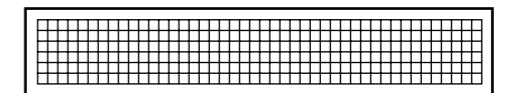


Standard Sizes

Unit Size	H	L	J	W	T	U	S
1	100	550	140	590	100	120	760
2	100	700	140	740	100	120	760
3	100	900	140	940	100	120	760
4	100	1000	140	1040	100	120	760
5	100	1200	140	1240	100	120	760

Optional Grilles: Eggcrate Pattern

Standard Supply: For Type SCTU Two no.





Description

The crosstalk attenuators are prefabricated sections of ductwork with acoustic lining.

It is designed to avoid noise radiated from a room or from a duct termination which is connected via a main duct, to a branch duct leading to another room. Airflow is permitted whilst noise transfer is limited.

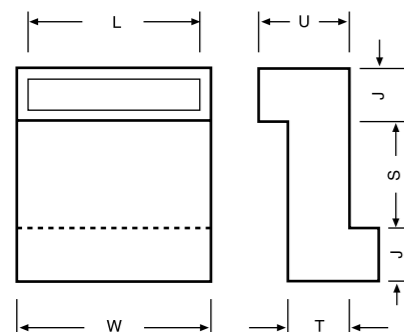
Construction

Type SCTZ attenuators have been designed to avoid noise interference between interconnected rooms. It is used as air transfer attenuators between adjoining areas where the acoustic integrity of a common partition or ceiling needs to be maintained.

Casing are manufactured from galvanized sheet metal Ga.20, with spot welded seams. The acoustic lining complies with Class O Building Regulations and has a glass tissue facing for erosion protection. The units may be supplied with one or two eggcrated grilles in natural anodised aluminium. Colour paint finishes are available to order.

Dimensions

Type SCTZ

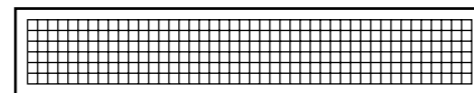


Standard Sizes

Unit Size	H	L	J	W	T	U	S
1	100	550	140	590	100	120	760
2	100	700	140	740	100	120	760
3	100	900	140	940	100	120	760
4	100	1000	140	1040	100	120	760
5	100	1200	140	1240	100	120	760

Optional Grilles: Eggcrate Pattern

Standard Supply: For Type SCTZ Two No.



- SCT 100 - 1
- SCT 100 - 2
- SCT 100 - 3
- SCT 100 - 4

Description

Prefabricated crosstalk attenuators Type SCTS and SCTBH with aerodynamic acoustic side liners has a high insertion loss designed to attenuate the airborne noise transmitted from a room to adjoining room through a duct termination which is connected to a common air duct system or through air transfer openings on walls or partitions. Crosstalk attenuator will allow to pass the required airflow whilst noise transfer will be limited meeting the designed noise level in the occupied space.

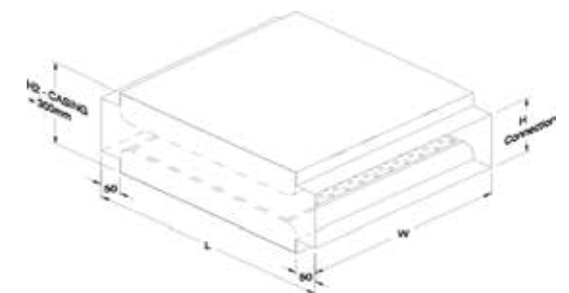
Construction

The casing and side liners are manufactured from galvanized sheet metal Ga.20. Casing is with lock formed seams, with mastic sealant. The construction complies with SMACNA and DW 144 standards. With spigot connections are supplied as standard.

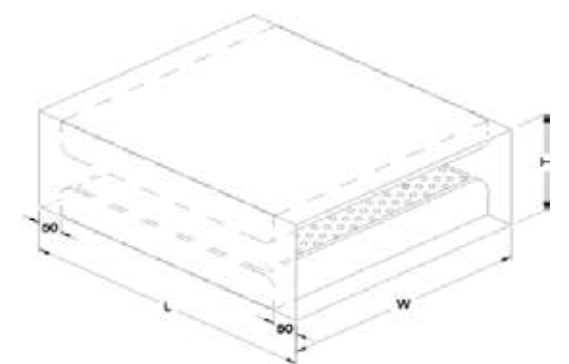
The aerodynamic acoustic side liners contain acoustic infill which complies with Class O Building regulations. The infill has a glass tissue facing and is contained behind galvanized perforated sheet metal. This dual protection prevents damage and fiber erosion up to 30 m/s airway velocity. The side liners are radiussed at both ends to minimize air pressure loss and regenerated noise.

Dimensions

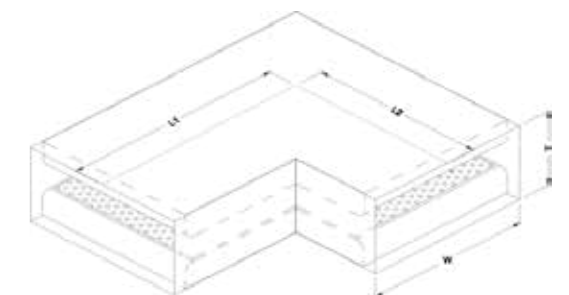
Type SCTS 100 - 1, SCTS 100 - 2, SCTS 100 - 3, SCTS 100 - 4



Type SCTS 100, SCTS 200



Type SCTS 100, SCTS 200
L = L1 + L2



ATTENUATOR PERFORMANCE

Type SCTL - SCTU - SCTZ

The acoustic performance of Type SCTL, SCTU and SCTZ is designed to maintain the acoustic integrity of a single thickness brick wall. Selection procedure is accordingly independent of source noise levels and noise requirements in the receiving room.

Pressure loss data includes an allowance for the use of standard eggcrate grilles. Alternative grille types are likely to increase resistance to airflow.

Table 2 incorporates guide figures from maximum pressure

loss against design noise level requirements, in order to limit attenuator self noise. These are shown as space noise criterion (NC) levels with 8dB room absorption.

Type SCTS and SCTBH

The acoustic performance of type SCTS and SCTBH is derived from tests meeting the requirements of BS 4718: 1971.

No deviations of insertion loss with airflow were recorded over the velocities employed in this brochure. The Static Insertion Loss figures are given in Table 3.

The total noise reduction figures shown in Table 3 gives an indication of the total room to room noise reduction that could be expected with a typical duct layout or with air transfer openings on walls or partitions. (Similar to Sound Reduction Index for a partition).

Table 5 incorporates guide figures for maximum duct velocity against design noise level requirements, in order to limit attenuator self noise. These are shown as space noise criterion

(NC) levels with 8dB room absorption. Full regenerated noise data for SCTS attenuators, is available upon request.

Pressure loss data assumes that the airflow to the attenuator is uniform over the face, in a duct-to-duct layout. Units installed in situations leading to poor inlet or discharge conditions could incur pressure losses higher than losses mentioned in the catalogue.

Table 1: Recommended Design Noise Criteria for Various Area Functions

Type of Room	NC
Section 1 - Studios and Auditoria	
Sound Broadcasting (general), TV (general), Recording Studio	20
TV (audience studio)	25
Concert Hall, Theatre	20 - 25
Lecture Theatre, Cinema	25 - 30
Section 2 - Hospitals	
Audiometric Room	20 - 25
Operating Theatre, Single Bed Ward	30 - 35
Multi-bed Ward, Waiting room	35
Corridor, Laboratory	35 - 40
Staff Room, Recreation Room	30 - 40
Section 3 - Hotels	
Individual Room, Suite	20 - 30
Ballroom, Banquet Room	30 - 35
Corridor, Lobby	35 - 40
Section 4 - Offices	
Boardroom, Large Conference Room	25 - 30
Small Conference Room, Executive Office, Reception Room	30 - 35
Open Plan Office	35
Drawing office, Computer Suite	35 - 45
Section 5 - Offices	
Bedroom	25
Living Room	30

SCTL, SCTU AND SCTZ

Method of Selection

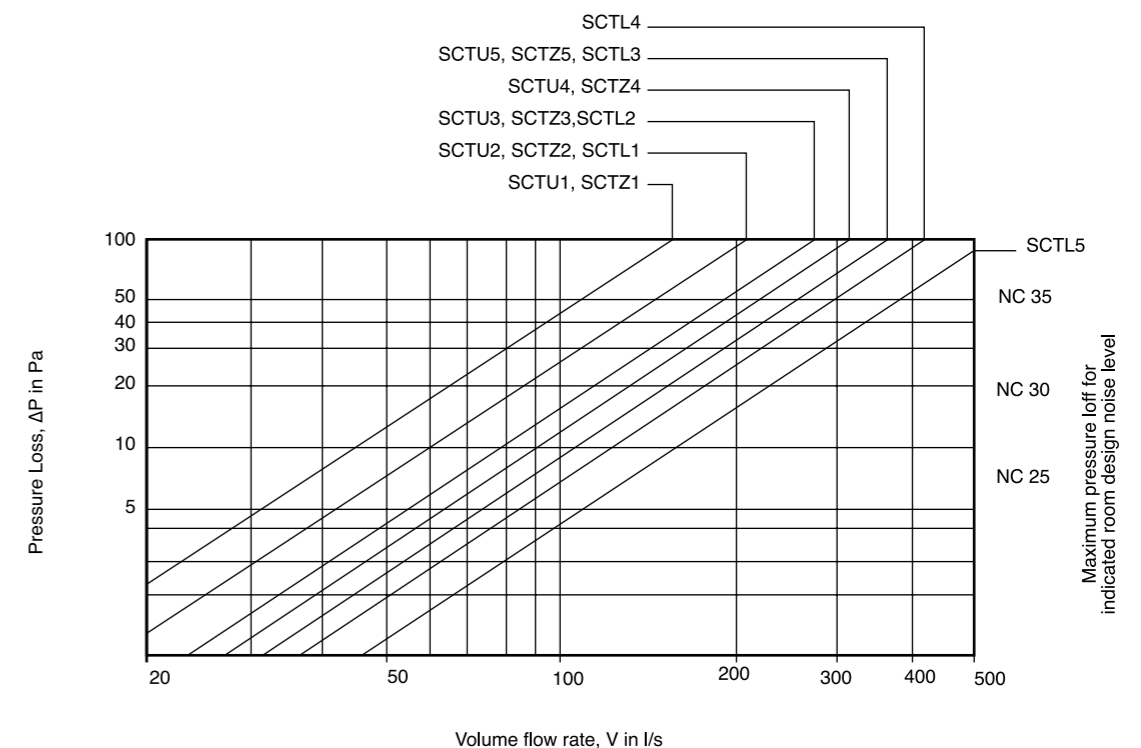
Type SCTL - SCTU - SCTZ

1. Select a suitable design NC level from Table 1.
2. For required volume flow rate, select from Table 2 a unit size for an acceptable pressure loss (typically 20 Pa).
3. Ensure that the pressure loss is kept within the guide limit for the design room NC level.
4. Check unit dimensions for each model. Situations leading to poor inlet or discharge conditions could incur pressure losses higher than losses mentioned in the catalogue.

Table 2: Pressure Loss for Indicated Room Design Noise Level Requirements

Nomenclature

- W in mm : Width inside duct.
- H in mm : Height in duct.
- L in mm : Length
- V in l/s : Volume flow rate.
- v_f in m/s : Face velocity based on $V \div (W \times H \times 1000)$.
- Δp in Pa : Pressure loss.
- f_m in Hz : Octave centre frequency.
- D_o in dB : Insertion loss.
- NC in dB : Noise criterion



SCT SERIES

Quick Selection

Type SCTS 100 - 1, SCTS 100 - 2, SCTS 100 - 3, SCTS 100 - 4

The quick selection method provides an attenuator selection for the control of speech crosstalk between rooms linked by a common duct system. The noise source has been taken as a "voice as loud as possible without strain" - approximately NC75/80dBA in a typical office environment. Attenuator length required depends upon the design background noise level for the receiving room.

1. Select a suitable design NC level from Table 1.
2. From Table 4 select the attenuator length shown against the NC level appropriate for the type of room being considered.
3. Using Table 5, select a cross section for the required volume flow rate and pressure loss/velocity. Discharge conditions could incur pressure losses higher than catalog.

Full Selection

Type SCTS 100 - 1, SCTS 100 - 2, SCTS 100 - 3, SCTS 100 - 4

When an attenuator performance requirement has been established following accurate acoustic analysis of source noise, transmission path and receiving room requirements, a suitable SCTS attenuator can be selected as follows.

1. From Table 3 select an attenuator length to meet the required insertion loss.
2. Check the Self Noise guide on Table 5 to determine the maximum velocity for the room NC level required (consult Table 1).
3. Using Table 5, select a cross section for the required volume flow rate and pressure loss/velocity.

Table 3: Insertion Loss (D_e in dB) - Type SCTS and SCTBH

Attenuator Length 'L' (mm)	Octave Centre Frequency (f _m in Hz)							
	63	125	250	500	1000	2000	4000	8000
500	5	7	10	15	23	17	13	11
750	6	9	14	23	37	29	22	16
1000	8	11	19	31	48	37	28	21
1250	9	14	23	38	50	44	32	26
1500	10	16	27	45	50	50	39	31

SCT SERIES

Table 4: Quick Selection

Design Noise Criterion in Noise Critical Area	Attenuator Length Required (mm)	Total Noise Reduction at 500 Hz (dB)
NC 45	500	20
NC 40	750	28
NC 35	1000	36
NC 30	1250	43
NC 25	1500	50

Table 5: Pressure Loss for Indicated Room Design Noise Level Requirements

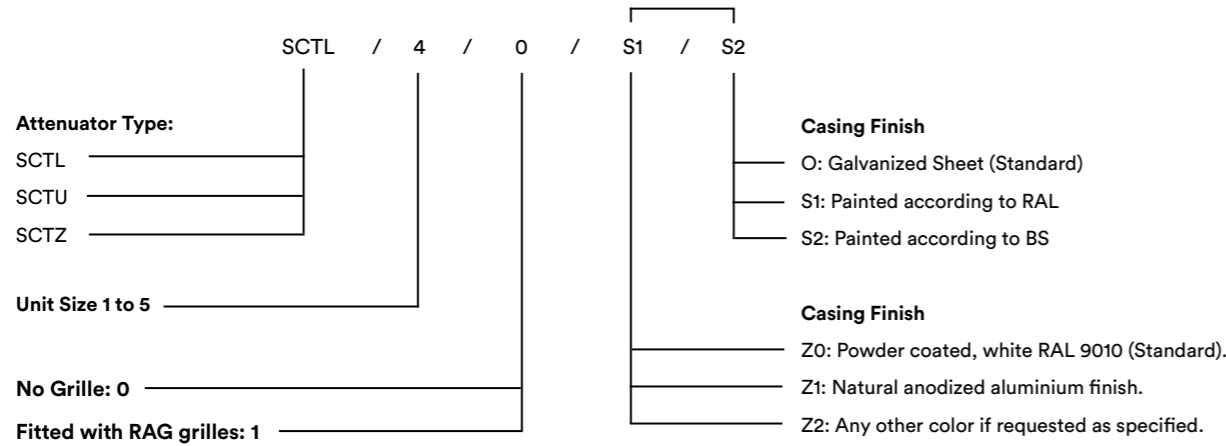
Attenuator Type	Air Velocity (v _i in m/s at duct size W x H)		2.0	3.0	4.0	5.0
	Self Noise Guide against Velocity		NC 25	NC 30	NC 35	NC 40
	Width 'W' (mm)	Height 'H' (mm)	Volume Flow Rate (litre/second)			
SCTS 100-1	100	100	20	30	40	50
	150	100	30	45	60	75
	200	100	40	60	80	100
Pressure loss (Δp in Pa)			< 5	< 5	6	10
SCTS 100-2	100	150	30	45	60	75
	150	150	45	70	90	115
	200	150	60	90	120	150
	250	150	75	115	150	190
	300	150	90	135	180	225
Pressure loss, (Δp in Pa)			< 5	8	14	22
SCTS 100-3	100	200	40	60	80	100
	150	200	60	90	120	150
	200	200	80	120	160	200
	250	200	100	150	200	250
	300	200	120	180	240	300
	350	200	140	210	280	350
	400	200	160	240	320	400
Pressure loss (Δp in Pa)			6	14	25	39
SCTS 100-4	100	250	50	75	100	125
	150	250	75	115	150	190
	200	250	100	150	200	250
	250	250	125	190	250	315
	300	250	150	225	300	375
	350	250	175	265	350	440
	400	250	200	300	400	500
	500	250	250	375	500	625
Pressure loss (Δp in Pa)			10	22	39	60

NOTE The total noise reduction at 500 Hz shown in Table 4 includes 5dB room absorption.

Order Details

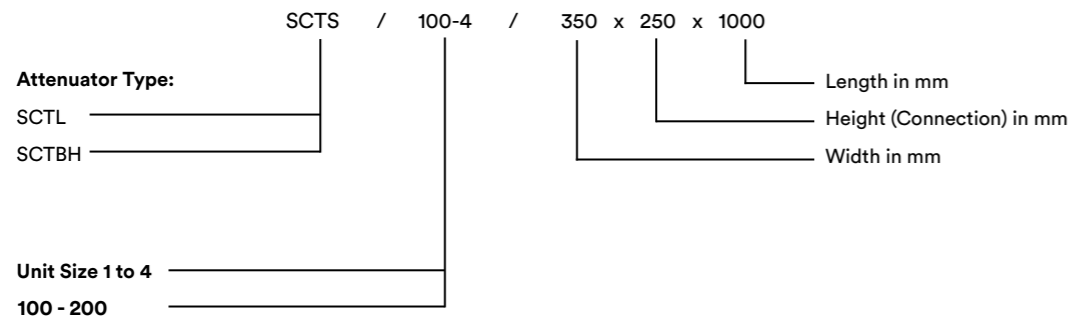
Order Code

For ceiling, wall/partition mounting attenuator:
These codes do not need to be completed for standard products.



Order Code

For ceiling, wall/partition mounting attenuator:



Specifications

Attenuator Type SCTL · SCTU · SCTZ

Type SCTL, SCTU or SCTZ crosstalk attenuator, incorporating erosion protected Class O acoustic infill. The casing is manufactured from Ga.20 galvanized steel sheet metal with spot welded seams.

Attenuators may be supplied with standard Return Air Grilles (RAG) if required.

For Duct, Wall/Partition Mounting:

Attenuator Type SCTS and SCTBH
Type SCTS or SCTBH crosstalk attenuator, incorporating aerodynamic side liners with erosion protected Class O acoustic infill covered by perforated

sheet metal. The attenuator casing is manufactured to DW 144 Class B medium pressure construction from Ga.20 galvanized steel sheet metal. The attenuators are provided with spigot end connections.

Order Example

For Ceiling Wall/Partition Mounting:

Make : SAFID
Type : SCTL-4/0
Qty : 1

For Duct Wall/Partition Mounting:

Make : SAFID
Type : SCTS 100-4 / 350 x 250 x 1000
Qty : 1

Fax Transmission & Post to: 00 966 1 460 0589

6 December 2001

C/01/5L/0121/L12AJTD/mth

Mr Jamal Jawhari
Saudi Air Distribution Systems Co. Ltd (SAFID)
P O Box 15300
Riyadh 11444
Kingdom of Saudi Arabia

Dear Mr Jawhari

Attenuator Tests - Catalogue Data

We have completed our calculations and extrapolations of the attenuator SIL test data. The table attached (Appendix A) contains the data for inclusion in the catalogue for the 4 types of attenuator SA20-75, SA20-100, SA20-150 and SA20-200's, for all lengths from 600mm to 2400mm.

The Static Insertion Loss, Generated Noise Level and Pressure Loss were tested in accordance with BS 4718:1971 "Methods of Test for Silencers for Air Distribution Systems". The standard lays down the methodology for taking measurements and calculating the values from those measurements and states the tolerances on the accuracy of the testing procedure.

The tables attached contain the relevant values taken from our laboratory test measurements and calculations/extrapolations and are adjusted in the normal fashion (eg. limiting the published Insertion Loss performance to 50 dB etc.)

The data for the catalogue (Appendix A) is attached.

If you have any questions please contact us.

Yours sincerely,



Jack Dalziel
Consultant
For and on behalf of
Sound Research Laboratories Ltd

Checked by,




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Appendix A

SA20-75 Attenuators

Length (mm)	63	125	250	500	1k	2k	4k	8k
0.6	9	13	22	36	45	39	33	29
0.9	10	16	27	41	49	47	38	33
1.2	11	18	31	46	50	50	43	38
1.5	12	21	36	50	50	50	48	42
1.8	13	24	41	50	50	50	50	46
2.1	14	26	45	50	50	50	50	50
2.4	15	29	50	50	50	50	50	50

SA20-100 Attenuators

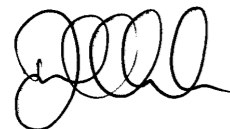
Length (mm)	63	125	250	500	1k	2k	4k	8k
0.6	7	10	18	34	46	40	33	29
0.9	8	12	22	37	50	46	36	31
1.2	9	14	26	40	50	50	39	33
1.5	9	17	30	44	50	50	41	35
1.8	10	19	34	47	50	50	44	37
2.1	11	21	38	50	50	50	47	39
2.4	11	24	42	50	50	50	49	41

SA20-150 Attenuators

Length (mm)	63	125	250	500	1k	2k	4k	8k
0.6	8	12	17	34	44	28	23	22
0.9	8	14	20	37	47	32	26	24
1.2	9	15	23	40	50	36	29	26
1.5	10	17	26	43	53	40	32	28
1.8	11	18	29	46	57	44	35	31
2.1	11	20	32	49	40	48	38	33
2.4	12	21	35	50	50	50	41	35

SA20-200 Attenuators

Length (mm)	63	125	250	500	1k	2k	4k	8k
0.6	7	11	16	25	27	23	21	20
0.9	8	12	18	30	33	26	23	21
1.2	8	14	21	35	39	30	25	23
1.5	9	15	23	40	44	33	28	24
1.8	9	17	26	45	50	37	30	26
2.1	10	18	28	50	50	40	32	27
2.4	11	19	30	50	50	43	34	28



Dave Clarke
Associate Director
For and on behalf of Sound Research Laboratories Ltd



Trevor Hickman
Executive Consultant





سافيد
SAFID

ACOUSTIC LOUVERS





Introduction

There are many applications in the industry where large quantities of air must be drawn from the atmosphere. The equipment handling the air is frequently noisy and it is necessary to provide some attenuation between the air moving device and the exterior. We have already seen that this can be done with cylindrical or rectangular sound attenuators. However, in certain conditions it is more appropriate to use an acoustic louver which is a combination of a normal louver, as associated with air inlets to buildings, and attenuator.

They are frequently installed in the facades of buildings where they are architecturally acceptable and yet provide an adequate amount of attenuation to prevent creating unacceptably high noise levels outside. Effectively, an acoustic louver is a very short attenuator with a very large cross-sectional area, so it is appropriate where length is restricted but face area is not.

Description

Acoustic louvers provide a positive solution where acoustic performance is required from a weather louver. The acoustic performance for an acoustic louver is usually measured in terms of transmission loss. This enables a direct comparison to be made between the performance of the louver and a solid wall which it probably replaces. Acoustic louvers as well as attenuators are frequently used in mechanical equipment rooms where a requirement for ventilation exists.

They are available in either steel or aluminum construction with standard and high acoustic performance options. A non-acoustic version having a complementary appearance is available and a variety of colored finishes may be specified.



Description

Type SALS acoustic louvers provide a positive solution where acoustic performance is required from a weather louver. They are available in either steel or aluminum construction with 'single' or 'double bank' acoustic performance options. A non-acoustic version having a complementary appearance is available. A variety of coloured finishes may be specified.

Construction

Steel Construction

Casings are manufactured from galvanized sheet metal channels Ga.16 minimum. Galvanized louver blades are of aerodynamic section and are set at approx. 40° on 150mm pitches. Bird screens from 12x12x1mm galvanized wire mesh are fitted as standard to all types, except Type SALN when fitted with blanking plate.

Acoustic louver blades contain infill which complies with Class O Building Regulations. The infill has a glass cloth facing and is contained behind perforated metal; this dual protection prevents damage and fibre erosion up to 30 m/s airway velocity.

Aluminum Construction

Construction is generally as for steel types described above except that the casing and louver blades are made from mill finish aluminum alloy, type 1050-H14.

Alternative Construction

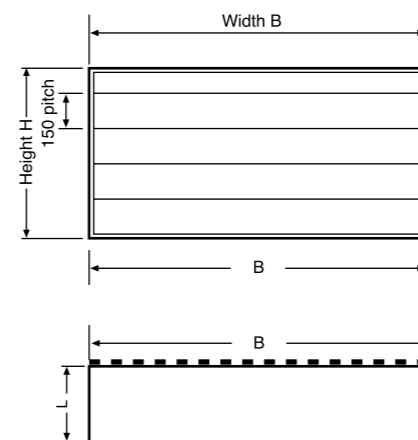
SALD

Type SALD; double bank acoustic louver comprising of two SALS type mounted back to back.

SALN

Type SALN; non-acoustic version with complementary appearance. Can be supplied with rear blanking plate to prevent air passage.

Dimensions

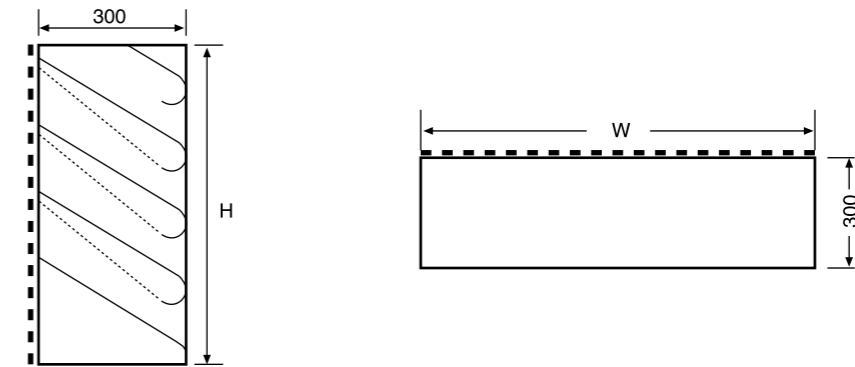


Dimensions in mm	Standard Sizes
W	300 to 1800 in increments of 150
H	450 to 2400 increments of 150

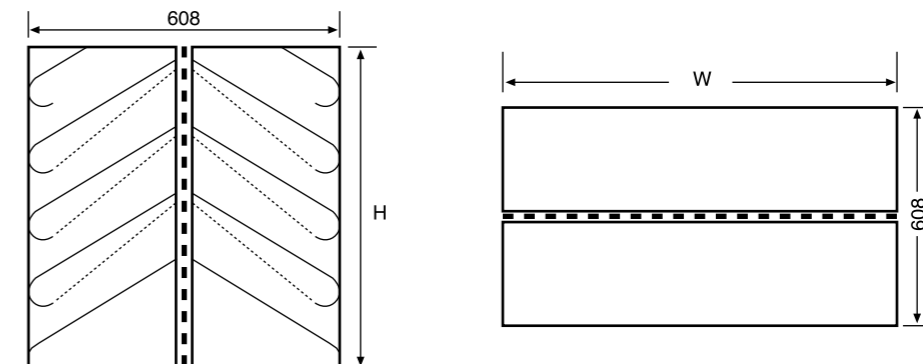
SALS, SALD AND SALN

Dimensions

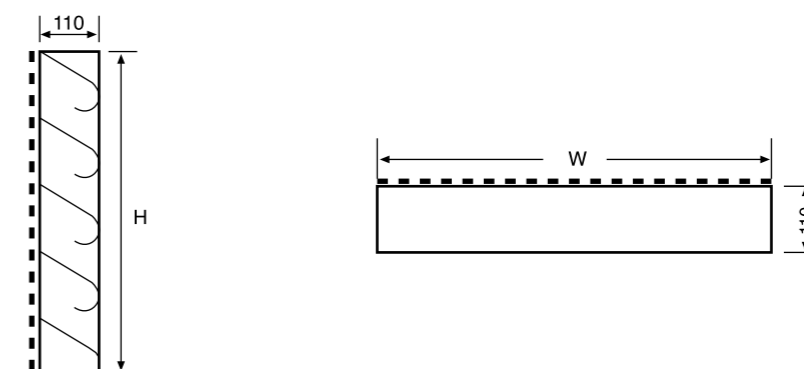
SALS



SALD



SALN



SALS, SALD AND SALN

Sectionalized Construction

Acoustic louvers are normally supplied in sections when either of the following dimensions is exceeded:

B = 1800 mm H = 2400 mm

Where louvers are in sections in both width and height, a 50x50x3 galvanized vertical box section frame is supplied to couple together adjacent sections. The weight of the upper section is borne by the coupling frame and not by the lower louver. Coupling frames are concealed behind a cover plate of material and finish to complement the louver.

The combinations illustrated on this page are available in louver Types SALS, SALD and SALN.

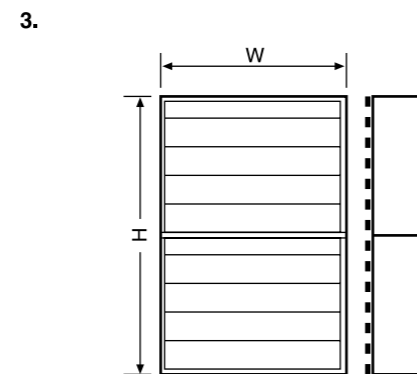
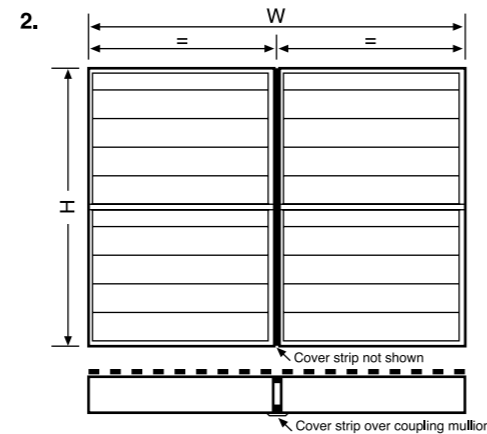
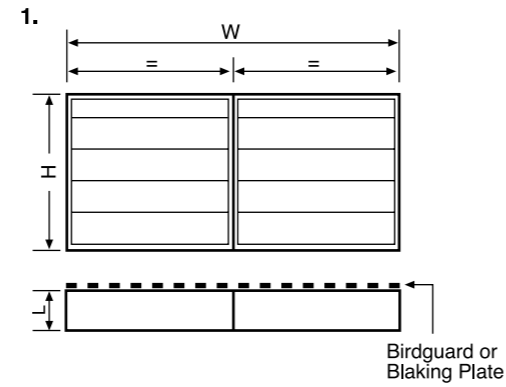
1. Split on width only.
2. Split on width and height.
3. Split on height only.

The assembly of sectionalised louvers is on site, by others. SAFID will provide full details of louver configuration and assembly.

Optional Features

Louvers can be supplied with matching sheet metal architrave or rolled metal angle picture frame. These would be supplied loose and undrilled for site fixing by others.

Dimensions



Installation

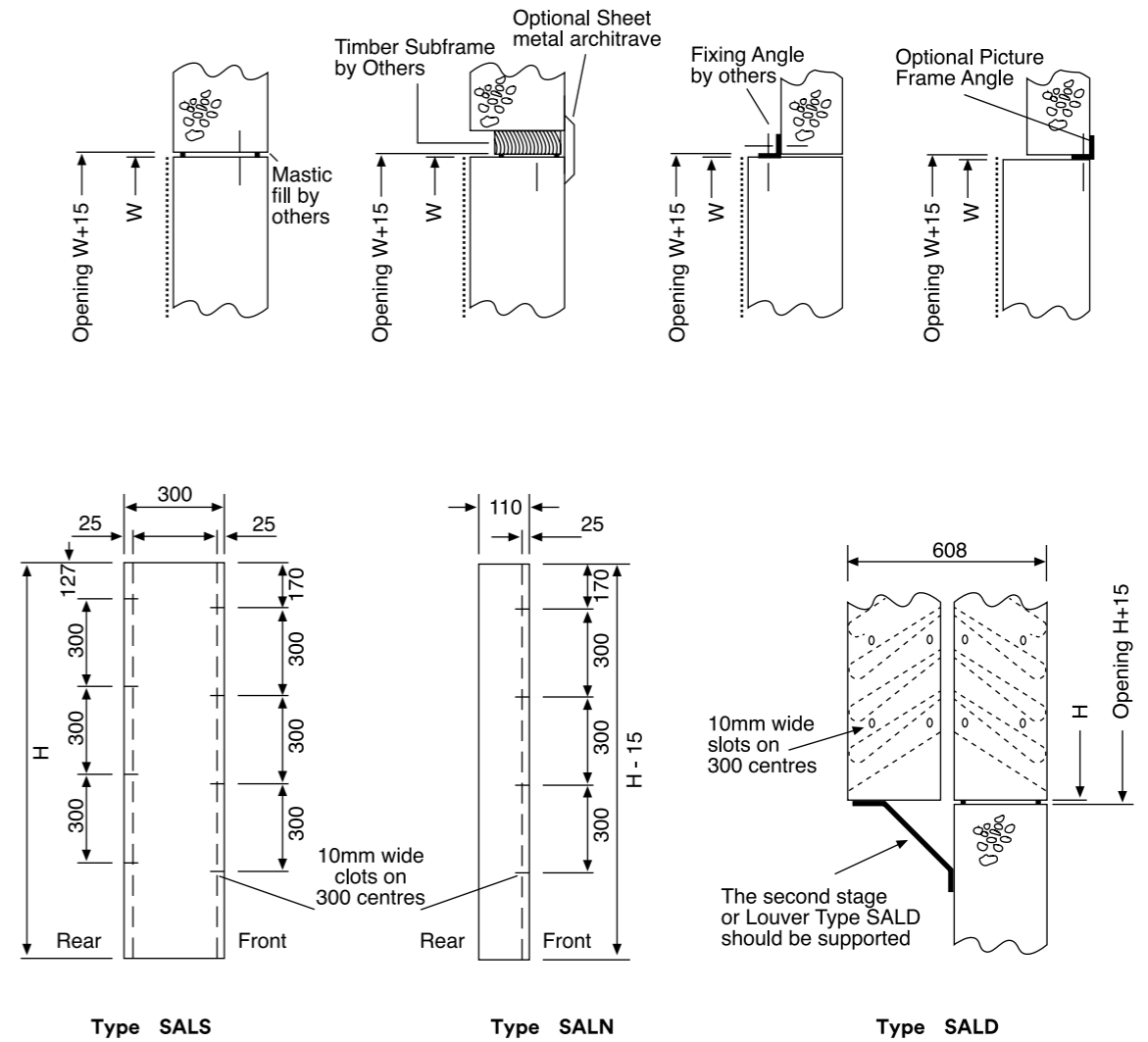
Type SALS, SALD, SALN

The vertical casing sides of the acoustic louvers are pre-slotted to facilitate fixing using a variety of acceptable methods. Where supplied, architraves and picture frames are supplied loose and undrilled.

On multisection units incorporating hollow section coupling frames, the frames are supplied drilled for easier site assembly. During fixing, the louvers should be set square and true in opening then wedged before fixing. Air gaps should be filled with a flexible mastic.

Installation and fixing items are not normally supplied; however, screws would be provided for use with our standard vertical box sections frames, where supplied.

Installation Details



Louver Selection

The acoustic performance needed to meet a particular design noise requirement can be calculated from other technical sources. Table 1 indicates the acoustic performance available from standard and high performance acoustic louvers.

From Table 2, select a louver size at a face velocity that gives an acceptable pressure loss. Check that louver self-noise will not infringe upon the design noise criterion by reference to the Self Noise Index, SNI.

The SNI gives an approximation of regenerated noise from the louver due to air velocity. This is expressed as an NC value at 1 meter, 3 meters and 10 meters from the louver face. The louver selected should have an SNI at least 5 NC below the design noise criterion.

Nomenclature

L in mm : Length (in direction of airflow)

W in mm: Width

H in mm: Height

V in l/s: Volume Flow Rate

V_f in m/s: Face Velocity based on $V \div (W \times H \times 1000)$

Δp in Pa: Pressure Loss

f_m in Hz: Octave Center Frequency

SRI in dB: Sound Reduction Index

SNI: Self Noise Index (equivalent to NC sound pressure level curve at free field distance shown)

Example

a) SRI Required @ f_m

63	125	250	500	1k	2k	4k	8k	Hz
3	5	7	11	14	16	10	8	dB

b) Design Noise Criterion = NC50 at 3 meters from opening.

c) Volume Flow Rate, V = 12000 l/s.

d) Maximum Required Pressure Loss, Δp=50Pa

e) Maximum Required Height, H = 1200mm.

1) From Table 1, a standard performance Type SALS louver would meet the required acoustic performance.

2) From Table 2, the maximum permissible face velocity, for Δp = 50 Pa, is 2.8 m/s.

3) From Table 2, the maximum permissible face velocity, v_f for an SNI of 50 minus 5 at 3m, is 4.9 m/s.

4) Size the louver at the limiting velocity of 2.8 m/s.

$$\begin{aligned} \text{Required Louver Ara (m}^2\text{)} &= V \div (v_f \times 1000) \\ &= 12000 \div (2.8 \times 1000) \\ &= 4.290 \end{aligned}$$

$$\begin{aligned} \text{Width (W Required)} &= 4.290 \div H \text{ (in meters)} \\ &= 4.290 \div 1.2 \\ &= 3.575 \text{ meters} \\ &= 3575 \text{ mm} \end{aligned}$$

Louver Selection:
Type SALS; W x H, 3575 x 1200
(Specify materials and Finish)

Acoustic Performance

Acoustic louver performance has been derived from tests based on BS 2750. The test work was carried out using a reverberant room technique. Measurements with and without the test piece were compared to produce the 'Sound Reduction Index' (also known as 'Transmission Loss') of both the 'single bank' performance SALS acoustic louver and the 'double bank' performance version SALD.

The term 'Noise Reduction' is sometimes encountered. This refers to free field measurements taken in close proximity to the louver face rather than in the reverberant receiving room described in BS 2750. This method tends to improve upon the Sound Reduction Index figures by 6 dB.

However, for most applications the 'Sound Reduction Index' data is the more appropriate, since for all practical purposes it may be used in the same way as the static insertion loss of a duct attenuator.

The aerodynamic profile of the acoustic louver blade ensures low pressure loss similar to conventional non-acoustic weather louvers of higher free area. The percentage free area varies with louver height, with the smaller louvers most affected by the restriction of the top and bottom dummy sections.

Weights

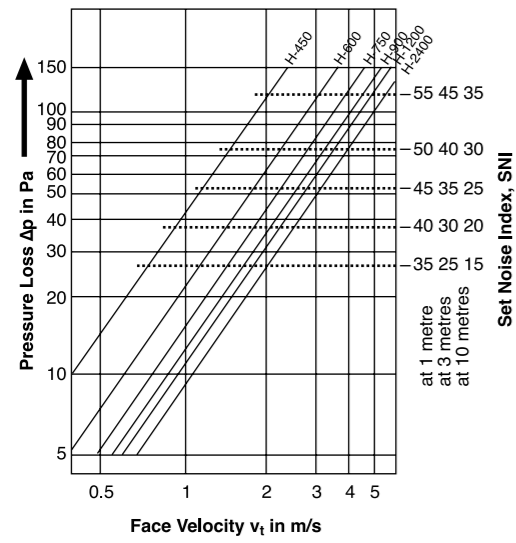
Louver Type	Approximate Weights
SALSS	48kg/m ² face area
SALSA	35kg/m ² face area
SALD	as SALSS or SALSA x 2
SALN	as SALSS or SALSA x 0.5

Table 1: Sound Reduction Index (SRI in dB)

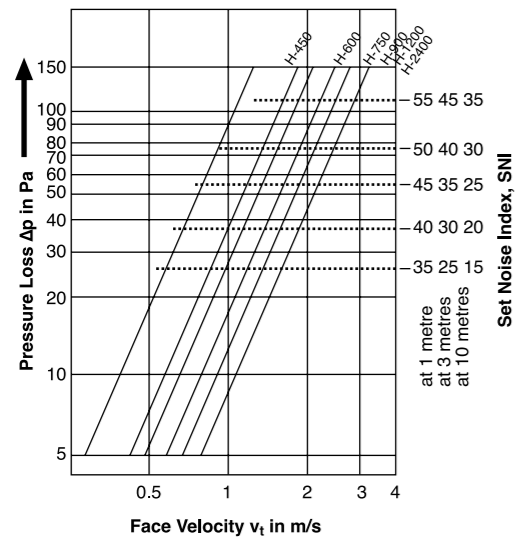
Louver Type	Octave Center Frequency f ^m in Hz							
	63	125	250	500	1k	2k	4k	8k
SALS	5	5	7	11	15	18	13	13
SALD	8	9	12	19	28	30	23	22

Pressure Loss and Regenerated Noise

Table 2:
Type SALS (ducted from atmosphere)



Type SALD (ducted from atmosphere)



Order Details

Specifications Text

Type SALS acoustic louver constructed from either galvanized sheet steel or natural mill aluminum with finish as specified. 1.5 mm thick channel casing incorporates aerodynamic acoustic blades containing erosion protected Class O infill covered by perforated sheet metal. Casing sides are pre-slotted for fixing into a prepared opening.

Ordering

Product Code: SAL D A 4000 1800

Type

Type Suffix:
 S - Single Bank
 D - Double Bank
 N - Non Acoustic

Material:
 S - Galvanized Steel
 A - Natural Aluminum

W (width, mm)
 H (height, mm)

